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PHOTOGRAPHIC EVALUATION REPORT MISSION 1019-1 29 APRIL - 4 MAY 1965

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TECHNICAL PUBLICATION

PHOTOGRAPHIC EVALUATION REPORT
MISSION 1019-1
29 APRIL - 4 MAY 1965

OCTOBER 1965

NATIONAL PHOTOGRAPHIC INTERPRETATION CENTER

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SYNOPSIS

Mission 1019-1 (System No. 1019-1) was launched 29 April 1965. Two periods of photographic operations (Missions 1019-1 and 1019-2) were executed as programmed, but an error in the re-entry sequence prevented recovery of the second film payload.

Mission 1019-1 (29 April-4 May 1965) accomplished 46 photographic revolutions, including 5 domestic and 5 engineering (dark-side) passes. The payload was recovered by air catch on 4 May. All cameras functioned satisfactorily throughout the mission. Telemetry indicated similar camera performances in the second phase, and it appears that only the re-entry sequence error prevented accomplishment of a successful 2-stage effort.

The panoramic records acquired in Mission 1019-1 were assigned a Mission Information Potential (MIP) rating of 85. The photography is comparable to that achieved in Mission 1015, flown 19-30 December 1964. However, the slave (AST) panoramic record is degraded by the presence of small, out-of-focus areas along the fiducial edge at both ends of the formats. A similar condition was reported in the evaluation of Mission 1015.

Clouds obscured 36 percent of the terrain covered in the mission. Solar elevation data are not available at this time.

GENERAL FLIGHT DATA

Launch Date 29 April 1965
Recovery Date 4 May 1965

Orbital Parameters
(Rev 41)

Period 91.069 Min
Perigee 99.772 nm
Apogee 259.83 nm
Eccentricity 0.0221
Inclination Angle 85.03° N

Photographic Operations

Operational Passes 38
Domestic Passes 5
Engineering Passes 5
Recovery Revolutions 80

PART I. CAMERA OPERATION

1. Master (FWD) Panoramic Camera No 118:

The instrument was operational throughout the mission and camera-induced film degradations consist primarily of various light-struck areas at the beginning and end of each pass record. Their appearances on the film conform to the following repetitive patterns:

(a) 1st frame: an equipment shadowgraph, not readily detectable in all passes.

(b) 5th-from-last frame: an edge-to-edge area of uniform fog, approximately 6 inches wide. This is reported to result from light passing through the vehicle's ablative shield.

(c) Next-to-last frame: a small light trace of irregular configuration, generally found on the fiducial edge at the take-up end of the format. This is the result of light passing through a drum leak and reflecting onto the film from a high-finish thermal surface in the barrel of the camera.

(d) Last frame: An equipment shadowgraph, present in most passes. Degradation of imagery within the affected areas is not severe except in the fifth-from-last frame where the uniform fogging occurs. The degree of degradation depends on solar elevation and azimuth and on the length of the camera-off period following termination of a photographic pass.

Intermittent minus-density streaks are noted in passes 1D and 3D. Their cause is unknown. Most of these streaks run roughly parallel to the major film axis through (or near) the frame centers. Some of the streak paths appear to coincide with field flattener movements, but others do not as readily conform to a possible relationship between the streaks and action of the field flattener.

Continuous rail scratches are present on both film edges. Most frames contain a group of short, fine, longitudinal emulsion scratches under the camera number and similar heavier scratches that extend from the take-up of the frame to the vicinity of the camera number. Although the latter are more prominent than have been observed in previous missions, degradation remains slight. Both types of scratches are tentatively identified as scan head roller scratches, caused during film transport as the scan arm returns to its start position.

2. Slave (AFT) Panoramic Camera No 119:

The unit was operational throughout the mission, and the majority of the camera-induced degradations are on the order of those noted in the fwd panoramic record. The most notable exception is the reappearance of an

out-of-focus condition which has not been observed since Mission 1015. Details of the more common light leaks, scratches, and so-forth will be cited after discussion of the focus anomaly.

The degraded areas are on the fiducial edge of the formats, in the vicinity of the shrinkage markers at the take-up and supply ends of the frames. Degradation is more consistent, and prominent at take-up. However, degradation at both ends of the formats is sometimes so subtle that detection is difficult, particularly when the imagery in the affected area does not contain sufficient culture for reference and comparison purposes. The size and contour of the out-of-focus areas vary but the estimated total image degradation within the individual frames does not exceed 1 percent. Obviously, however, the presence of a focus problem merits attention without regard to the physical extent of the degradation. Precise determination of the initial appearance of the out-of-focus condition in this mission was hampered by cloud cover and/or lack of culture in the early photographic passes, but there is evidence that the anomaly already existed in pass 2D and was possibly present as early as pass 2B.

Extensive investigation of previous mission records that contained similar degradations, such as Missions 1004, 1007, 1010, 1011, and 1015, indicates a possible relationship between format pitch (the alignment of the individual formats relative to the major axis of the film) and the presence of the out-of-focus condition. Apparently, pitch variations are a significant factor. In addition, it appears that a critical displacement between the pitch of the supply and take-up format ends must occur in order to induce degradation.

No focus anomaly is detectable in the fwd panoramic record acquired in this mission. The format pitch measurements are relatively stable throughout the entire record, and the difference between the pitch measurement at supply and pitch value at take-up of any individual frame seldom exceeds 0.010 inch. (Pitch is measured from the fiducial edge of the format to the edge of the film, at points immediately adjacent to and inboard of the end shrinkage markers.)

The aft pitch measurements exhibit considerable instability, as does the differential between the supply and take-up ends of the formats. Sample pitch values and pertinent comments follow:

Pass	Average Pitch At Take-up (inches)	Average Pitch At Supply (inches)	Average Differential (inches)	Comments
1D	0.24	0.255	0.010	Imagery does not permit positive detection of degradation.
2D	0.235	0.245	0.010	
5D	0.230	0.245	0.015	Small degradation at take-up.
8D	0.230	0.245	0.015	Same as in 5D.
9D	0.230	0.245	0.015	Same as in 5D and 8D.
13D	0.232	0.247	0.015	Degradation slightly larger.
19D	0.240	0.250	0.010	Degradation decreased.
21D	0.230	0.245	0.015	Degradation increased.
22D	0.232	0.247	0.015	Same as in 21D.
23D	0.230	0.247	0.017	Degradation slightly more prominent.
24D	0.235	0.252	0.017	Same as in 23D.
25D	0.242	0.253	0.011	No apparent change.
30D	0.242	0.257	0.015	Small degradation detectable both ends.
41D	0.237	0.257	0.020	Degradation more pronounced at supply.
57D	0.240	0.255	0.015	Degradation at take-up much increased, extends approximately 1/2 inches along format edge and intrudes 1/4 inch into format at maximum penetration point.
62D	0.245	0.257	0.012	Degradation reverts to previous small extent.
63D	0.242	0.255	0.013	No apparent change at take-up or supply.

Certain conclusions may be drawn from the above tabulations and comments but caution is advised. The pitch measurements were obtained with a 7X monocular fitted with a 0.005 inch reticle. In addition to the obvious limitations of the instrument itself, there is the possibility of human error in taking off the values. Furthermore, it is difficult to detect the presence of degradation and even more difficult to assess its extent where no culture or prominent terrain features are imaged. Bearing these factors in mind, the following conclusions are offered:

(a) There is a critical displacement ratio (pitch at take-up versus pitch at supply) which must be attained in order to induce a detectable out-of-focus condition. Maximum degradation in this mission is observed in pass 57D (which, coincidentally, contains a high culture content) and the pitch readings at take-up averaged 0.240 inch while the supply pitch values averaged 0.255 inch. Although the differential between take-up and supply (0.015 inch) is present in other passes, in no other case is the degradation observed to be as extensive.

(b) The differential between the 2 ends of the format is also a potent factor. Refer to pass 41D, where the difference is 0.020 inch and degradation is not only readily detectable at both ends but now appears to be more prominent at supply.

(c) Finally, it appears that pitch displacement ratio and pitch differential must combine in a critical relationship of values in order to induce maximum degradation. A shift in this relationship will alter the degree and even the location of the out-of-focus condition within a frame.

The aft panoramic record contains a number of light-struck areas similar to those present in the fwd material. However, the repetition pattern differs slightly:

(a) 1st frame: an equipment shadowgraph appears in a few passes.

(b) 6th-from-last frame: an edge-to-edge area of uniform fog, approximately 6 inches wide.

(c) 2nd/3rd-from-last frames: a light trace between the frames which may shift into the supply end of the 3rd-from-last frame or to take-up of the 2nd-from-last frame. An equipment shadowgraph occasionally appears in the 2nd-from-last frame.

(d) Last frame: an equipment shadowgraph is present in a number of passes, and a bar-type light trace is detectable in a few passes.

The same camera-induced scratches noted in the fwd panoramic record are present in the aft material. A continuous plus-density streak runs through the frame-centers of pass 4D. Minus-density streaks are intermittent and few.

transverse banding is detectable in pass 2-D and becomes progressively greater in subsequent passes. As in previous missions, the banding is most prominent at the start of the scan action and is derived from non-linear movement of the scan head with relation to the film. Degradation is not severe.

3. Master (FWD) Horizon Cameras:

The port (supply) and starboard (take-up) horizon cameras were operational throughout the mission. Exposure was adequate except where low solar elevations precluded effective horizon photography. Image quality is good.

4. Slave (AFT) Horizon Cameras:

The port (take-up) and starboard (supply) horizon cameras functioned satisfactorily. Exposure was adequate except where low solar elevations prevailed. Image quality is similar to that obtained with the master horizon cameras.

5. Stellar Camera No 15:

The instrument performed without malfunction and produced good-quality images. All of the stellar frames were used to advantage in the vehicle attitude analysis. It is believed that the attitude values obtained from each frame are correct. As a matter of interest, it is noted that the horizon reduced values do not square with the stellar reductions. With reference to roll, for example, the horizon reductions indicate twice as much roll (in terms of actual minutes of arc) as the stellar reductions reveal.

The geometric distribution of the stellar images (approximately 30 readily identifiable stars) is good. Images are detectable even in the format areas degraded by earth albedo. Albedo degradation, incidentally, appears to be of less magnitude than in most previous missions.

Approximately 25 frames contain stellar images which are distorted to some degree. The factors which contribute to the distortions (streaking, elongation, and so forth) are not precisely known, but it is currently felt that timing conditions in the panoramic cameras and monoscopic operations in certain circumstances are involved.

6. Index Camera No D35:

The unit was operational throughout the mission and produced good-quality photography, perhaps the best obtained to date.

7. Associated Equipment:

The binary data block failed to record on 6 frames, as follows:

Pass 8D, frame 31 (fwd)
Pass 21D, frame 103 (fwd)
Pass 30D, frame 17 (fwd)
Pass 68D, frame 15 (aft)
Pass 72D, frame 70 (aft)
Pass 74D, frame 12 (aft)

In addition, the uniform fog present in certain frames of the panoramic photography (See Items 1 and 2 of this part) caused the dot reader to make erroneous interpretations of the binary data a number of times during the binary readout.

The frequency marks are flared, but the marks and attendant reflected images are recorded outside of the formats. However, intensity of the marks is not consistent, and they often range from underexposed to adequately exposed within a pass. The end-of-pass markers are heavily overexposed. The horizon format fiducials are slightly flared throughout the fwd panoramic material. One of the horizon fiducials is similarly affected in the aft panoramic record (the fiducial adjacent to the panoramic frames in the starboard horizon formats). The camera number is slightly flared, and the adjacent binary index lamp is considerably bloomed.

FIGURE 1. DESCRIPTION OF PHOTOGRAPHIC DATA

The data pertaining to photographs contained in this publication are defined as follows:

PASS: A pass is the operational portion of an orbital revolution. The suffix D indicates that the photography was acquired during the descending portion. Suffix A indicates that the photography was acquired during the ascending portion, and suffix M indicates that the photography was acquired during a pass that includes both ascending and descending portions. An additional suffix, E, indicates that the pass was an engineering operation or that a portion of the pass has been edited.

DATE OF PHOTOGRAPHY: The date of photography indicates the day, month, and year (GMT) that the photography was acquired.

UNIVERSAL GRID COORDINATES: These coordinates are included to locate the illustrated photography within the panoramic format.

ENLARGEMENT FACTOR: The enlargement factor is included to indicate the number of diameters the original material has been enlarged in the photographic illustration.

GEOGRAPHIC COORDINATES: These coordinates are included to indicate the latitude and longitude of the panoramic format.

ALTITUDE: This measurement is the vertical distance from the vehicle to the Hough Ellipsoid at the time of the acquisition of the photography.

PITCH: Rotation of the camera about its transverse axis. Using appropriate aeronautical terminology, positive readings indicate nose-up attitude and negative readings indicate nose-down attitude.

ROLL: Rotation of the camera about its longitudinal axis. Using appropriate aeronautical terminology, positive readings indicate left wing-up attitude and negative readings indicate right wing-up attitude.

YAW: Rotation of the camera about its vertical axis. Positive readings indicate counterclockwise rotation when viewing the ground nadir from the vehicle-mounted camera in-flight.

LOCAL SUN TIME: This time is included to present to the viewer a realistic time of acquisition of the photography illustrated.



FIGURE 2. EXAMPLE OF HORIZON CAMERA PHOTOGRAPHY

NPIC R-8028 (10/68)

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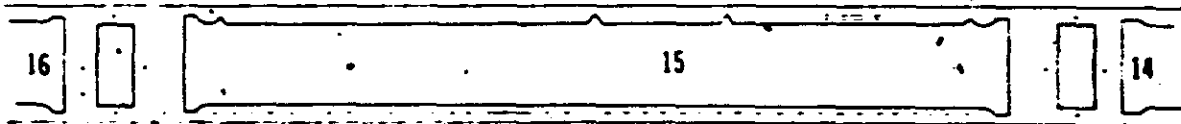
Pass STD F&D
Frame 15
Date of Photography 3 May 1965
Universal Grid Coordinates Starboard Horizon
Enlargement Factor 3X
Pan Format Geographic Coordinates 52-16N 13-30E
Altitude (feet) 631, 605
Camera Attitude
Pitch 14°56'
Roll 00°10'
Yaw 00°13'
Local Sun Time 1309 hours
Solar Elevation 50°59'
Solar Azimuth 153°
Exposure f/3.0 @ 1/100 sec

Approximate flight direction
on photograph



Approximate scan direction
on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.



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FIGURE 3. EXAMPLE OF STELLAR CAMERA PHOTOGRAPHY

NPIC K-9030 (10 68)

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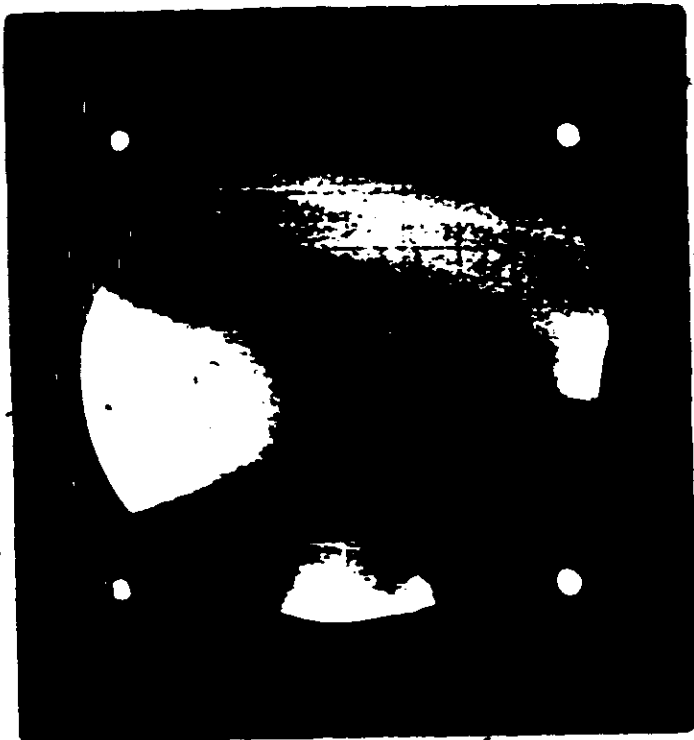


Stellar Frame Number 303
Correlates with FWD Camera:
 Pass 57D
 Frame 15
Date of Photography 3 May 1965
Enlargement Factor 3X
Pan Camera Attitude:
 Pitch 14°56'
 Roll 00°10'
 Yaw 00°15'
Exposure Time 1/1.3 @ 2 sec

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FIGURE 4. EXAMPLE OF INDEX CAMERA PHOTOGRAPHY

NPIC N-0031 (10/88)

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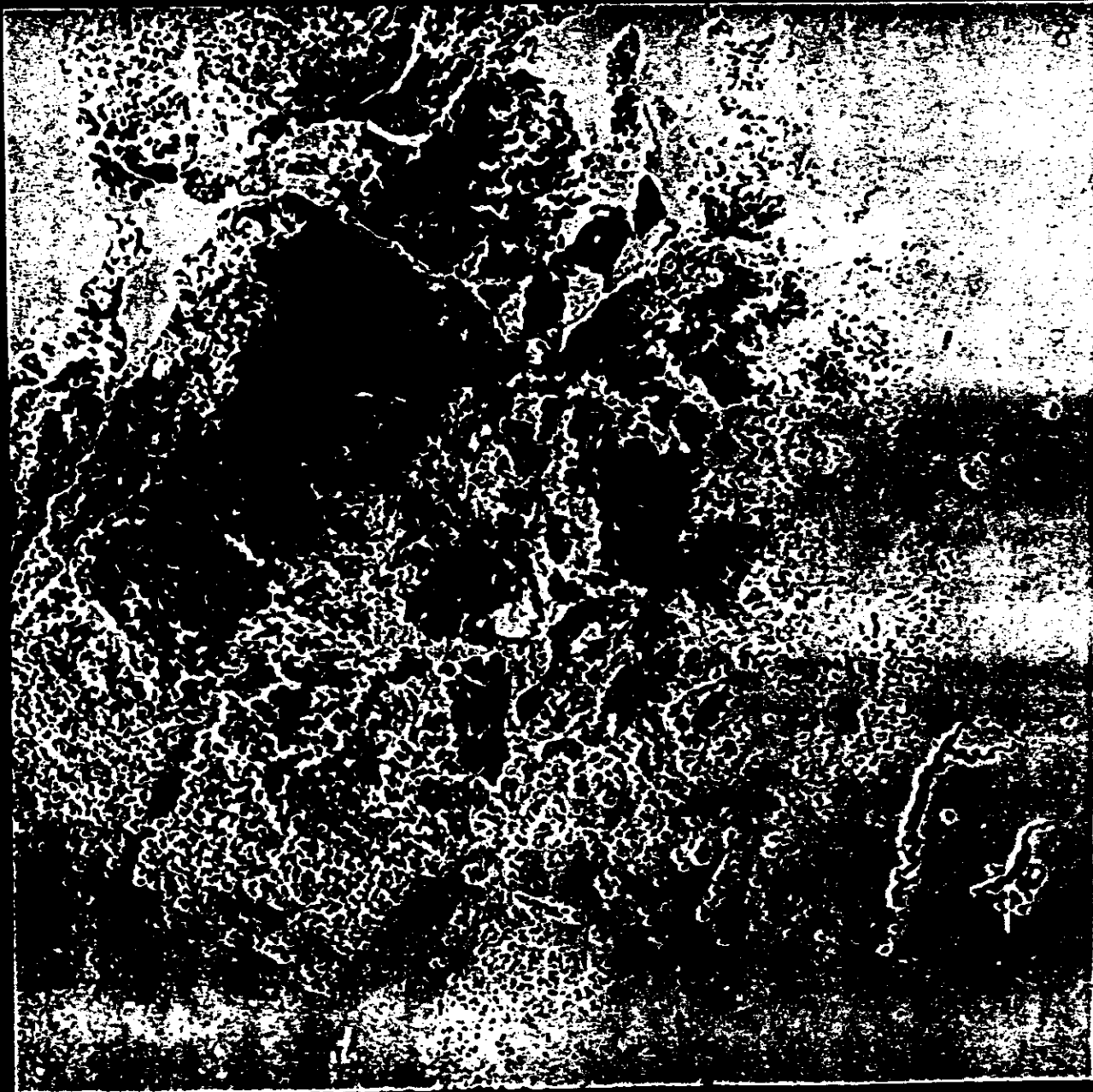
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Index Frame Number 308
Correlates with FWD Camera:
 Pass 57D
 Frame 15
Date of Photography 3 May 1965
Enlargement Factor 3X
Pan Camera Attitude:
 Pitch 14°56'
 Roll 00°10'
 Yaw 00°15'
Exposure 2/4.5 @ 1/500 sec

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FIGURE 5.. EXAMPLE OF OUT-OF-FOCUS CONDITION IN APT PANORAMIC PHOTOGRAPHY

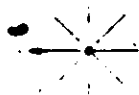
MPIC X-0032 (10/68)

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Pass. 57D AFT
Frame 25
Date of Photography 3 May 1965
Universal Grid Coordinates 62.5 - Take-up End of Frame
Enlargement Factor Contact
Geographic Coordinates 51-36N 13-33E
Altitude (feet) 627, 442
Camera Attitude Vehicle:
Pitch Not Available
Roll Not Available
Yaw Not Available
Local Sun Time 1310 hours
Solar Elevation 51°33'
Solar Azimuth 153°
Exposure 1/376 sec

The overlay defines the approximate contour of the out-of-focus condition in this frame. Precise outline of the degradation is difficult to accomplish, due to the illumination fall-off in this area, with resultant general loss of image quality.

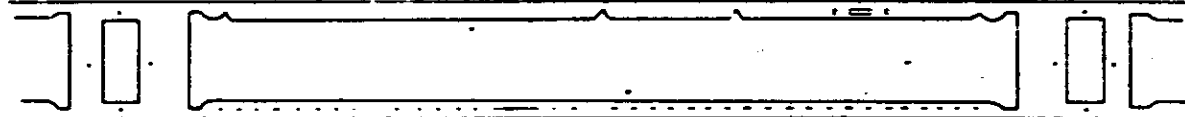


Approximate flight direction on photograph

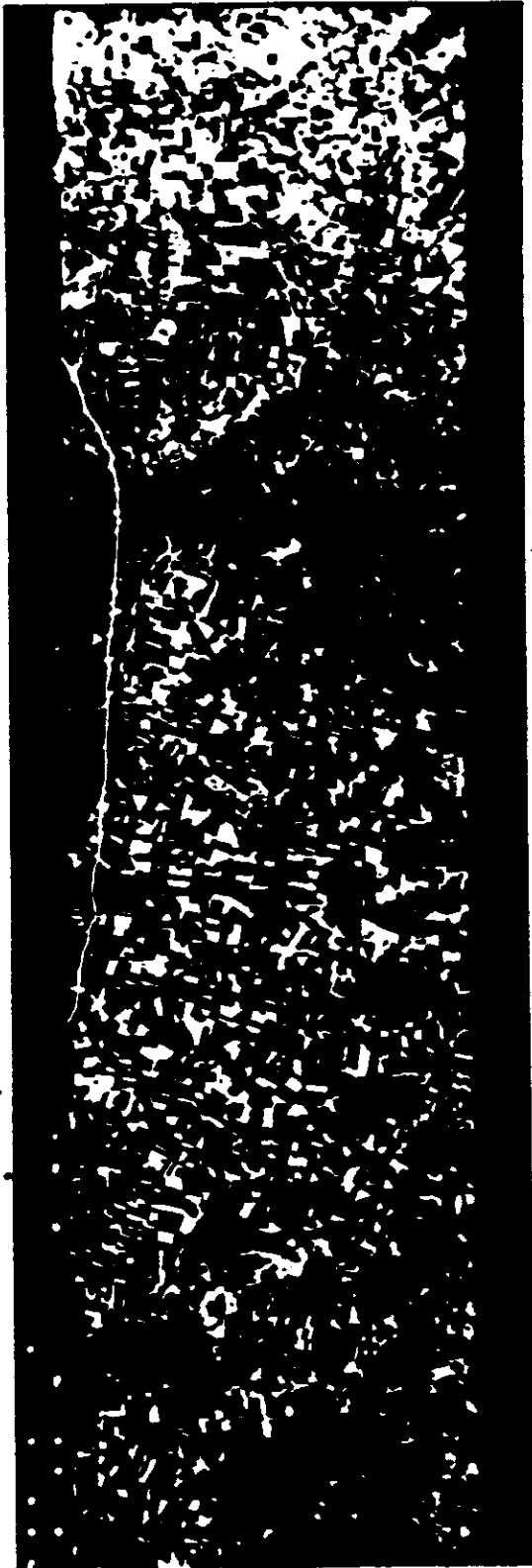


Approximate scan direction on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.



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PART II. FILM

1. Film Footage/Frame Totals:

The film footage/frame totals for Mission 1019-1 are as follows:

Master (FWD) Panoramic Camera	7,254 ft/2,829 frames
Slave (APT) Panoramic Camera	7,842 ft/2,779 frames
Stellar Camera	54 ft/ 401 frames
Index Camera	90 ft/ 401 frames

Total Panoramic Footage/Frames 15,096 ft/5,000 frames

(Note: All footage figures are process machine footages.)

2. Film Processing:

This section provides evaluation of processing, density, contrast, and physical condition of the original negatives. Processing data are abstracted from records maintained by the processing contractor. Evaluation of exposure and physical condition of the film are accomplished by on-site inspection of the negative material as it is made available for breakdown and titling. A final, more thorough examination of the original negative is conducted by photographic analysts at a later date.

In general, most of the photography obtained in this mission received adequate exposure. However, low solar elevations and/or variations in terrain reflectivity caused some departures from normal. Densities range from thin (in photography acquired at low solar elevations) to heavy. The majority of the density values (approximately 50 percent) fall in the medium category. Similarly, most of the photography contains medium-contrast imagery.

The following development levels were employed in processing the film:

	<u>Master</u>	<u>Slave</u>
Primary	22%	25%
Intermediate	32%	55%
Full	46%	19%

Sixty-four processing level changes were required for the master (fwd) panoramic record and 41 changes for the slave (aft) material. Three parts required special printing.

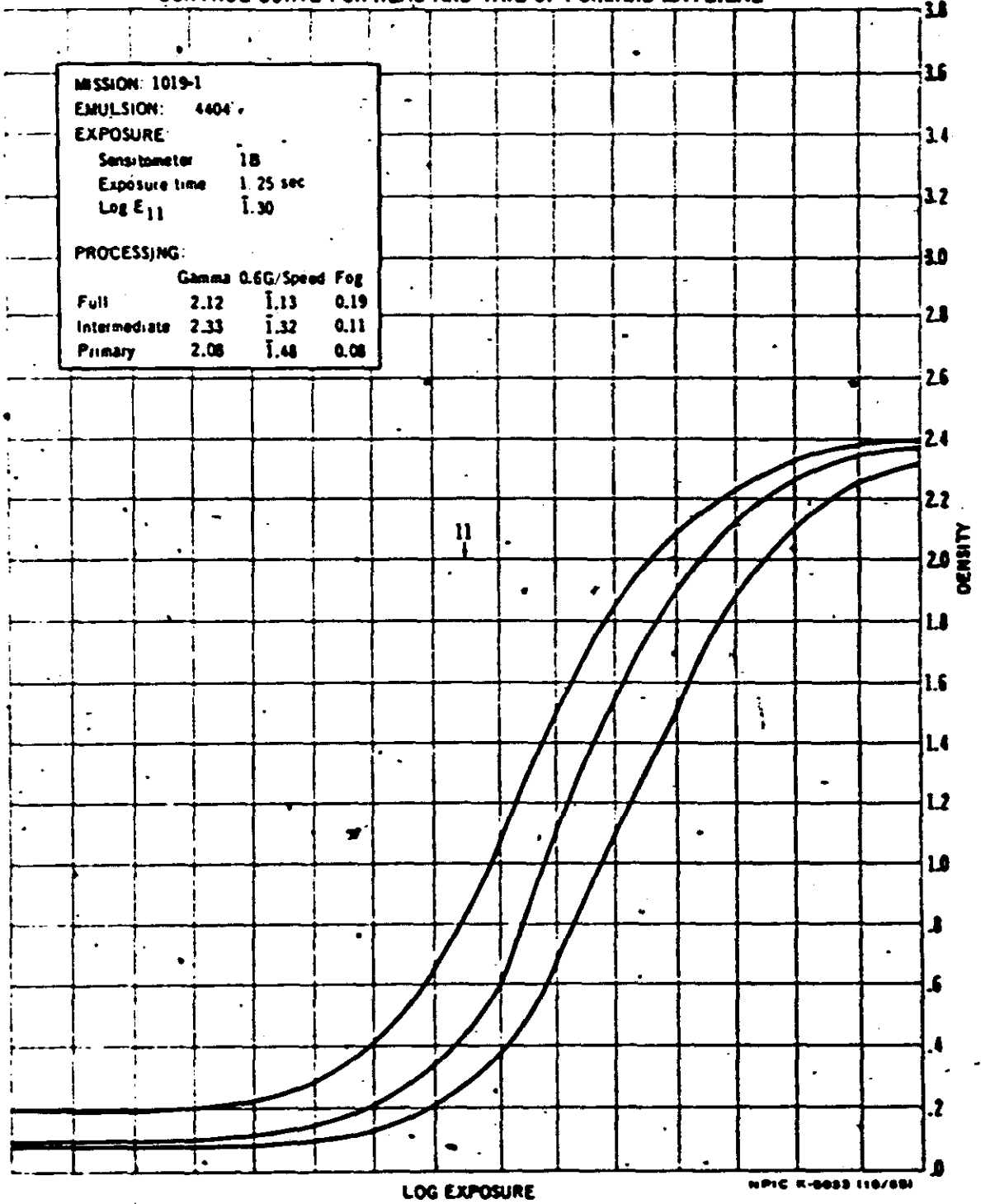
3. Physical Film Degradations:

Pass 5D, frame 112 (fwd) contains numerous transverse emulsion scratches. Similar, heavier scratches are present in pass 23D, frame 45 (fwd) near frame-center. In pass 21D (fwd), frames 20-137 are degraded by numerous, small longitudinal emulsion scratches. Continuous heavy, parallel base scratches are present in pass 41D, frames 46-50 (aft).

4. Film Processing Curves:

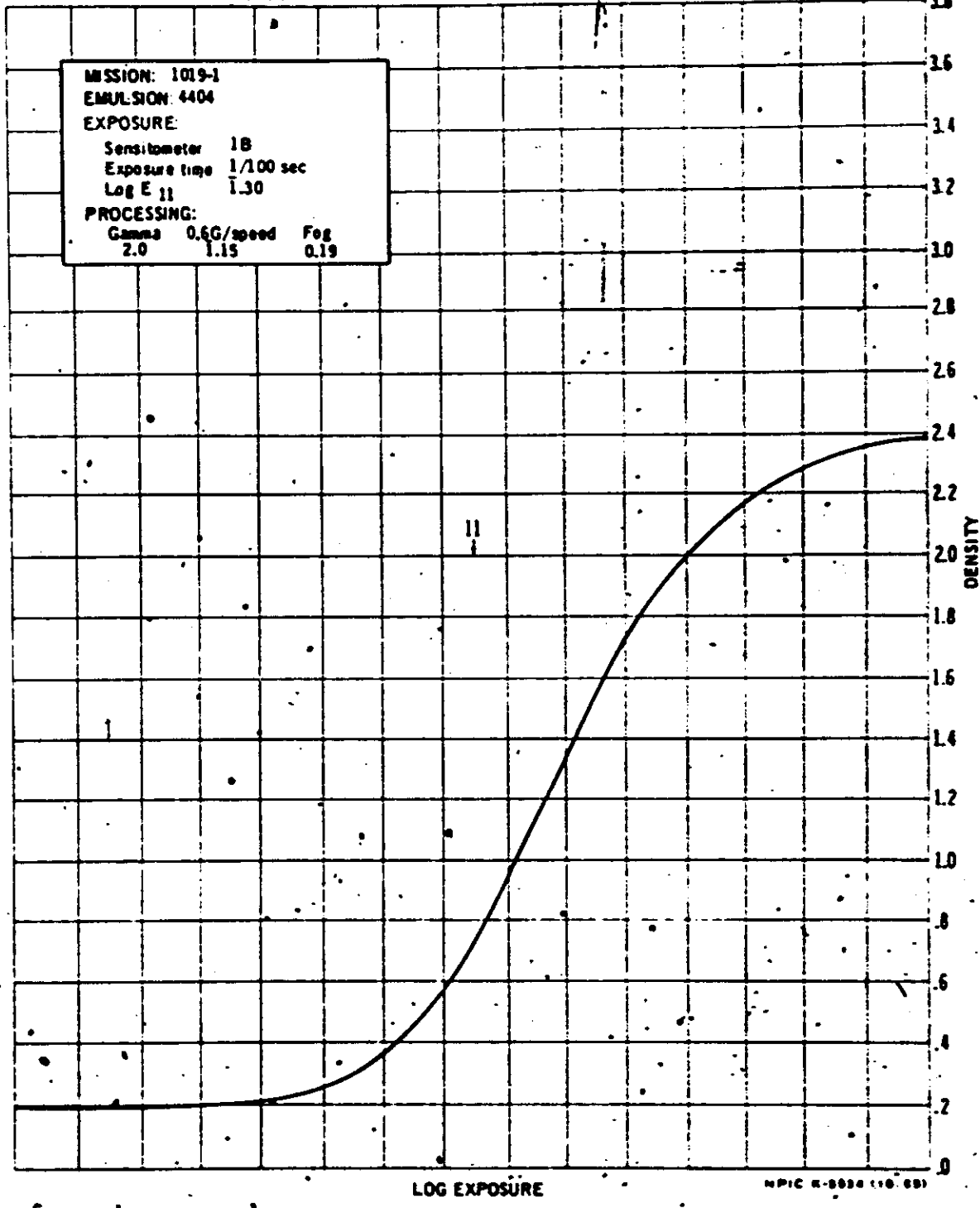
The following graphs are reproductions of the film processing curves provided by the processing contractor for Mission 1019-1.

CONTROL CURVE FOR HEAD AND TAIL OF FORWARD MATERIAL





CONTROL CURVE FOR HEAD AND TAIL OF FORWARD MATERIAL

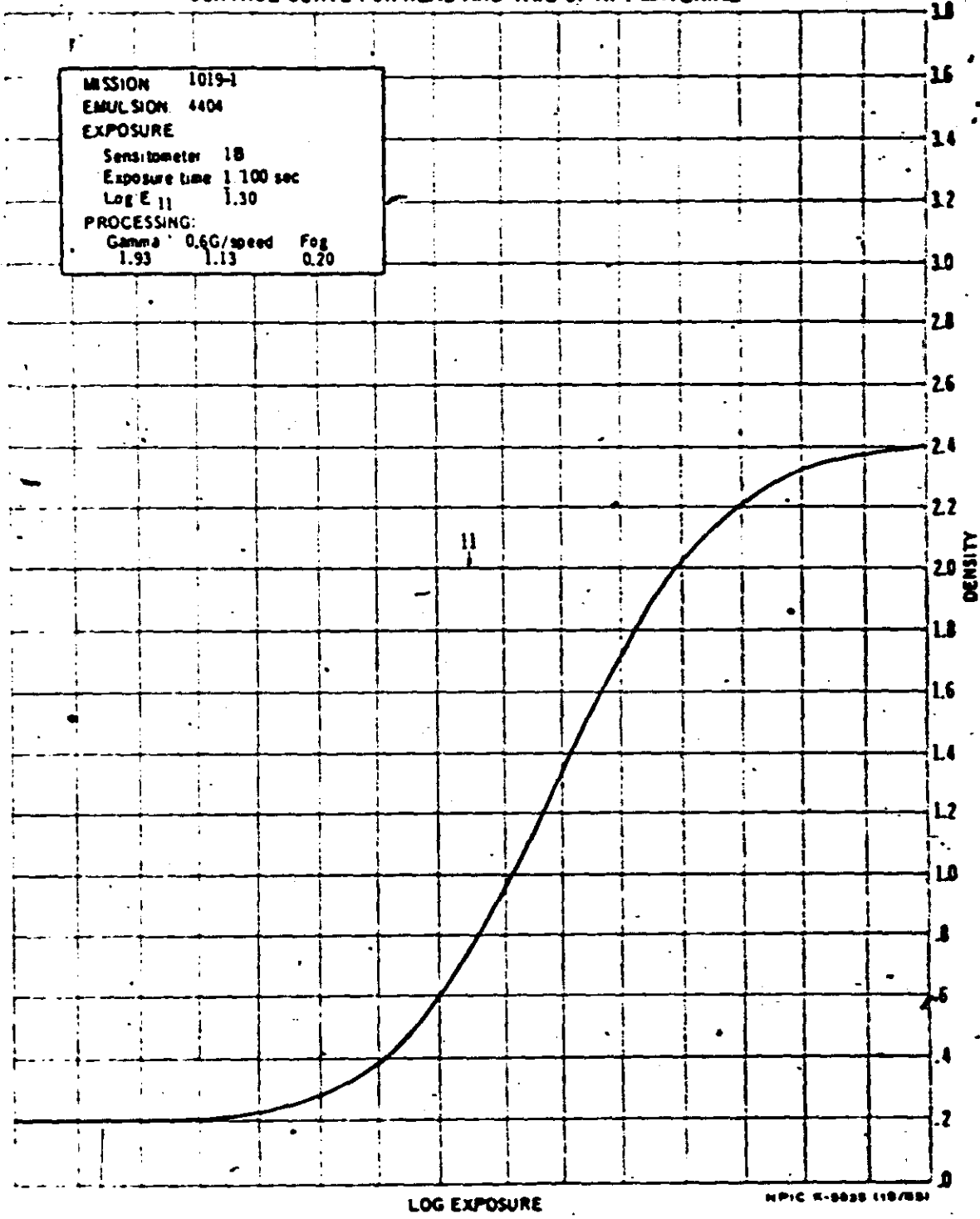


MISSION: 1019-1
EMULSION: 4404
EXPOSURE:
Sensitometer 1B
Exposure time 1/100 sec
Log E 11 1.30
PROCESSING:
Gamma 0.6G/speed Fog
2.0 1.15 0.19

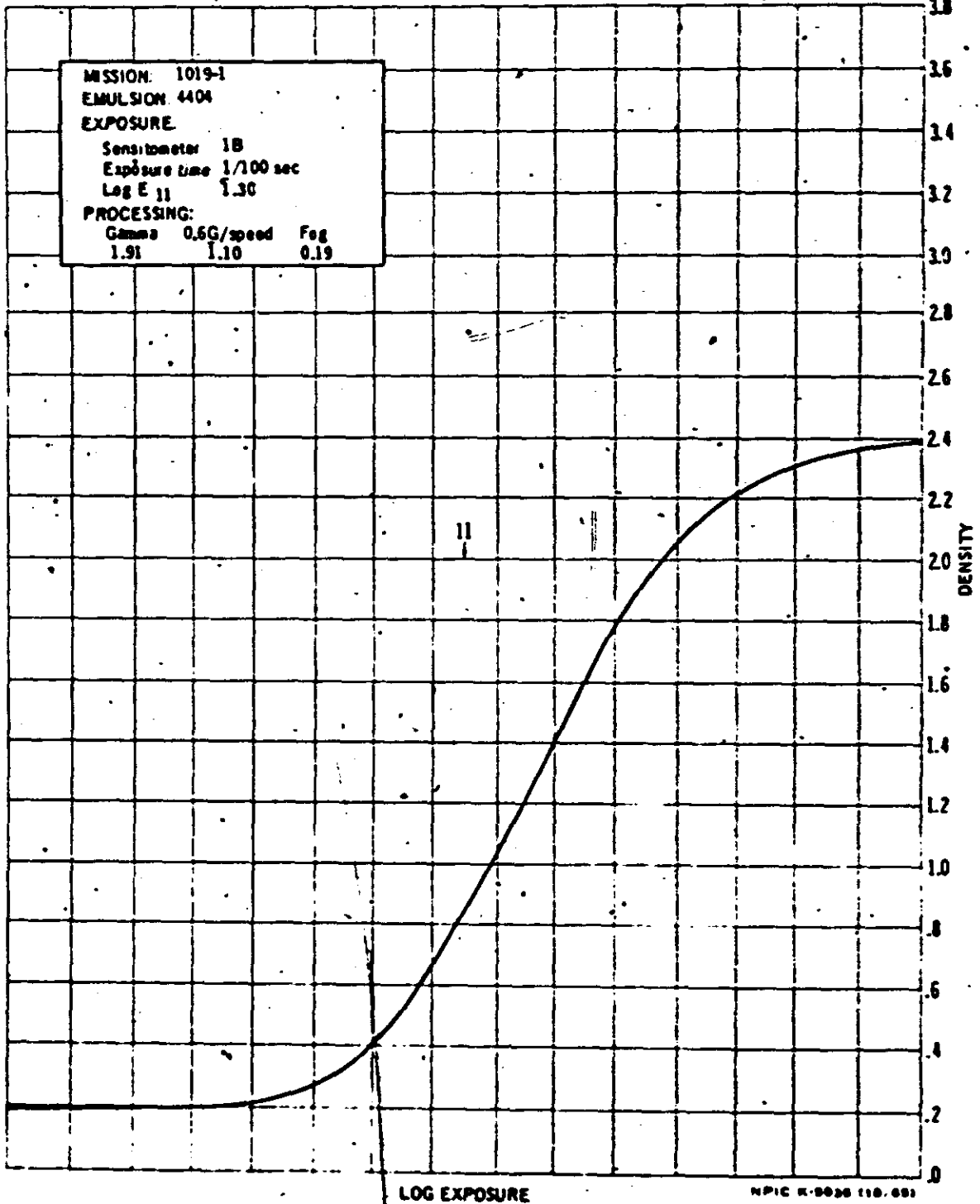
LOG EXPOSURE

NPIC R-0000 (10/00)

CONTROL CURVE FOR HEAD AND TAIL OF AFT MATERIAL

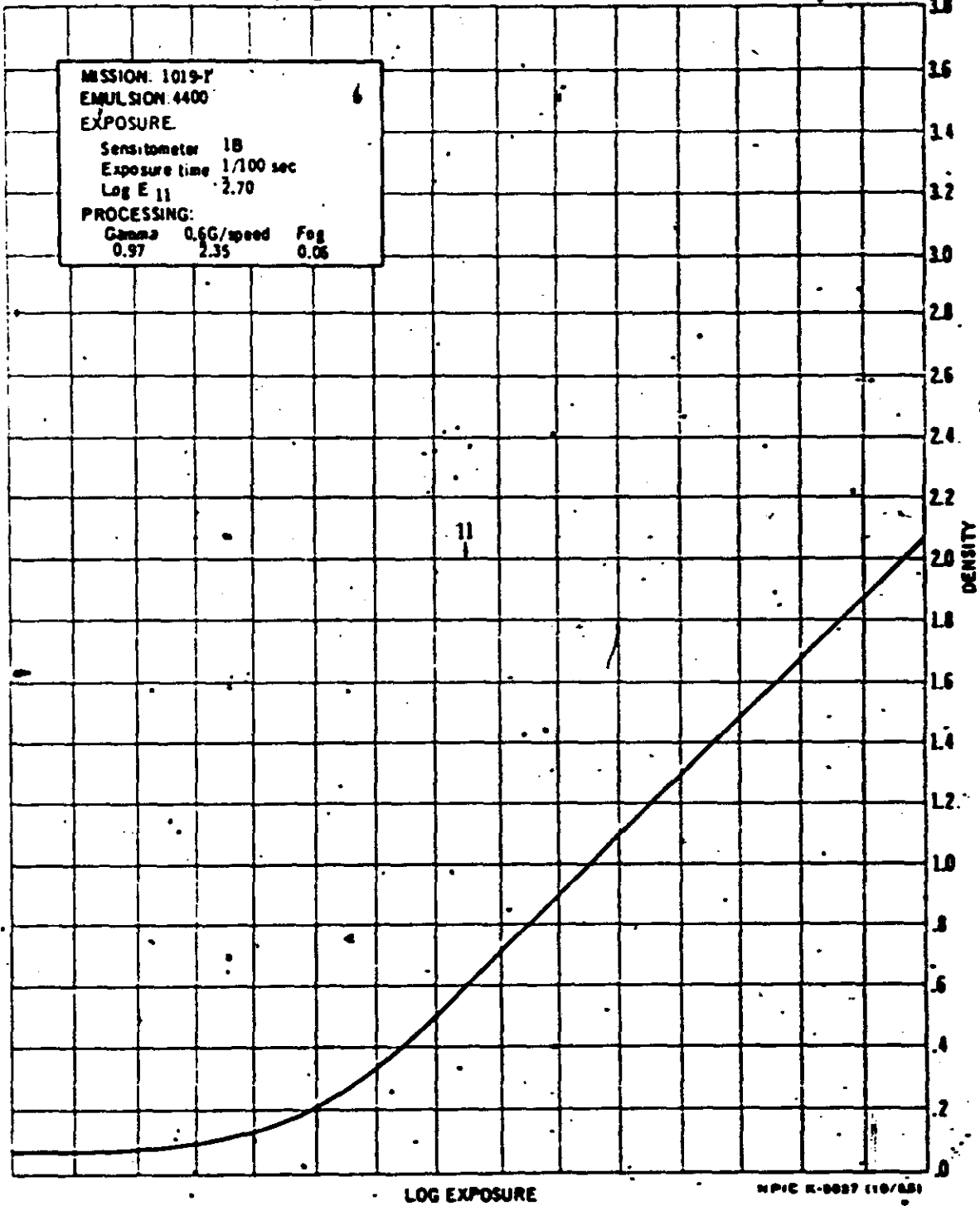


SENSITOMETRIC CURVE FROM MISSION MATERIAL





CONTROL CURVE FOR HEAD AND TAIL OF FORWARD MATERIAL



PART III. IMAGE QUALITY

1. Definition of Photographic Interpretation (PI) Suitability:

This is an assessment of the information content of photographic reconnaissance material and its interpretability. A number of inter-related factors are involved, such as the quality of the photography, the extent of target coverage, scale, and weather limitations. However, the criteria for assigning a PI suitability rating may be reduced to (a) the scope of the photographic coverage and (b) the degree to which a photo interpreter may extract useful and reliable information from the material.

PI suitability ratings are categorized as Excellent, Good, Fair, Poor, and Unusable. These ratings refer to the overall interpretive value of the photography obtained from a particular reconnaissance mission. Individual targets may also be assigned PI suitability ratings if that is necessary or desirable. The standards that determine assignment of the various ratings are as follows:

Excellent: The photography is free of degradation by camera malfunctions or processing faults and weather conditions are favorable throughout. The imagery contains sharp, well-defined edges and corners, with no unusual distortions. Contrast is optimal and shadow details, as well as details in the highlight areas, are readily detectable. Observation of small objects and a high order of mensuration are made possible by the consistently superior quality of the photography.

Good: The photography is relatively free of degradations and limiting weather conditions. Edges and corners of objects are well-defined. No unusual distortions are present. Detection and accurate mensuration of small objects is feasible, but to a lesser degree than in material rated as "Excellent."

Fair: Degradation is minimal but the acuity of the photography is less than optimal. Edges and corners of objects are not crisply defined and there is loss of detail in shadow and/or highlight areas. Detection and identification of small objects is possible but accuracy of mensuration is reduced by the less-than-optimum contrast that prevails.



Poor: Camera-induced degradations and/or weather limitations severely reduce the quality of the photography. Definition of edges and corners is not sharp. Only gross terrain features and culture may be detected or identified and distortion of form may exist. Accurate mensuration of even large objects is doubtful.

Unusable: Degradation of the photography completely precludes detection, identification, and mensuration of cultural details.

2. PI Suitability, Mission 1019-1:

The PI suitability of Mission 1019-1 ranges from fair to good. The photographic coverage affords observation of 71 targets. A few of the coverage highlights reported in the preliminary readout are:

- (a) Possible new electronics facility under construction at a nuclear weapons proving ground.
- (b) Identification of 2 new fixed field missile sites.
- (c) New identification of a probable missile training site.
- (d) Confirmation of a previously suspect nuclear weapons storage area.

Interpretation of approximately 30 percent of the targets was hampered by unfavorable atmospheric conditions in the target areas. Low contrast and/or obliquity further complicated observation in a number of cases. Cloud reflectance streaking is detectable in portions of the photography, but the attendant degradation is not significant. (This anomaly was discussed in some detail in the report on Mission 1015.)

The initial scan of the mission record was performed in a relatively short time, without the aid of the precise analytical and mensuration instruments normally employed. Continued study of the film may reveal additional targets and may alter some of the information obtained during the initial interpretation phase.

3. Definition of Mission Information Potential (MIP):

The MIP is an arbitrary number, not limited by terminal values, which is subjectively assigned to the panoramic photography of a mission and which compares it to the other missions. It is meant to be a measure of the camera's maximum capability for recording information, discounting adverse atmospheric conditions, minimum solar elevations, camera malfunctions, or other factors which reduce the quality of the photography.

The MIP is based on the best photography found in a mission, even though the photography may be limited to a few frames. Since these frames are considered to be the best in the mission, they do not indicate the overall success, average quality, or general interpretability of the photography.

Criteria for selection of the MIP frame:

- a. Eliminate all portions of the mission affected by system malfunctions.
- b. Select frames which are free of clouds or atmospheric attenuation.
- c. Eliminate the first 10 frames and last frame of a pass because these may be affected by incorrect scan speed.
- d. Select frames that are in a continuous strip of approximately 10 cloud-free frames because cloud shadows from weather fronts are cast for great distances.
- e. Determine from the horizon cameras that the panoramic photography is not affected by apparent vehicle perturbations.
- f. Select targets that are near the center of the format and on frames as close as possible to perigee for scale purposes and to eliminate obliquity.
- g. Select frames having near optimum solar elevation.
- h. Select a high-contrast target (preferably an airfield) and compare the target to a previous mission which has been given an MIP rating.

4. MIP, Mission 1019-1:

Based on the foregoing criteria, the airfield near frame-center of frame 14 in pass 57D (fwd) is selected as the MIP example for this mission and is assigned a rating of 85. In general, the photographic quality of the master (fwd) panoramic record is judged to be slightly better than that of the slave material but the difference is neither consistent nor uniform when evaluated on a frame-for-frame basis. The overall quality of the panoramic records is considered comparable to Mission.1015, 19-30 December 1964.

Handle Via
~~Talent-KEYHOLE~~
Control System Only

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~



FIGURE 6. MIP SELECTION, MISSION 1019-1.

NPIC N-8038 (10-88)

- 20a. -

~~TOP SECRET RUFF~~
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Control System Only

Pass 57D FWD
Frame 14
Date of Photography 3 May 1965
Universal Grid Coordinates 44.5 - 13.4
Enlargement Factor 20X
Geographic Coordinates 52-27N 13-28E
Altitude (feet) 632, 021
Camera Attitude:
Pitch 14°57'
Roll 00°09'
Yaw 00°17'
Local Sun Time 1309
Solar Elevation 30°52'
Solar Azimuth 153°
Exposure 1/254 sec



Approximate flight direction
on photograph



Approximate scan direction
on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.





Handle Via
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Control System Only

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~~NO FOREIGN DISSEM~~

FIGURE 7. EXAMPLE OF MASTER (FWD) PANORAMIC CAMERA PHOTOGRAPHIC QUALITY

REF ID: A66118/688

20c

~~TOP SECRET RUFF~~
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Handle Via
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Talent-257001E
Control System Only

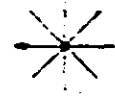
~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~



Pass 57D F&D
Frame 12
Date of Photography 3 May 1965
Universal Grid Coordinates 42.1 - 11.6
Enlargement Factor 20X
Geographic Coordinates 52-45N 13-25E
Altitude (feet) 632, 865
Camera Attitude:
Pitch 14°58'
Roll 00°06'
Yaw 00°14'
Local Sun Time 1309
Solar Elevation 50°37'
Solar Azimuth 153°
Exposure 1/254 sec



Approximate flight direction
on photograph



Approximate scan direction
on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.



~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~

Handle Via
Talent-257001E
Control System Only



CONFIDENTIAL
EXCLUDED FROM AUTOMATIC
DOWNGRADING AND
DECLASSIFICATION

TOP SECRET//SI//
TK//SI

FIGURE 1. Example of a data visualization of a complex system

TOP SECRET//SI//
TK//SI

Handle Via
Talent REFLECT
Control System Only

~~TOP SECRET RUFF~~
NO FOREIGN DISSEM



Pass	57D AFT.
Frame	18
Date of Photography	3 May 1965
Universal Grid Coordinates	48.7 - 10.4
Enlargement Factor	20X
Geographic Coordinates	52-41N 13-22E
Altitude (feet)	630, 221
Camera Attitude	
Pitch	Not Available
Roll	Not Available
Yaw	Not Available
Local Sun Time, A	1309
Solar Elevation	50°40'
Solar Azimuth	153°
Exposure	1/376 sec



Approximate flight direction
on photograph



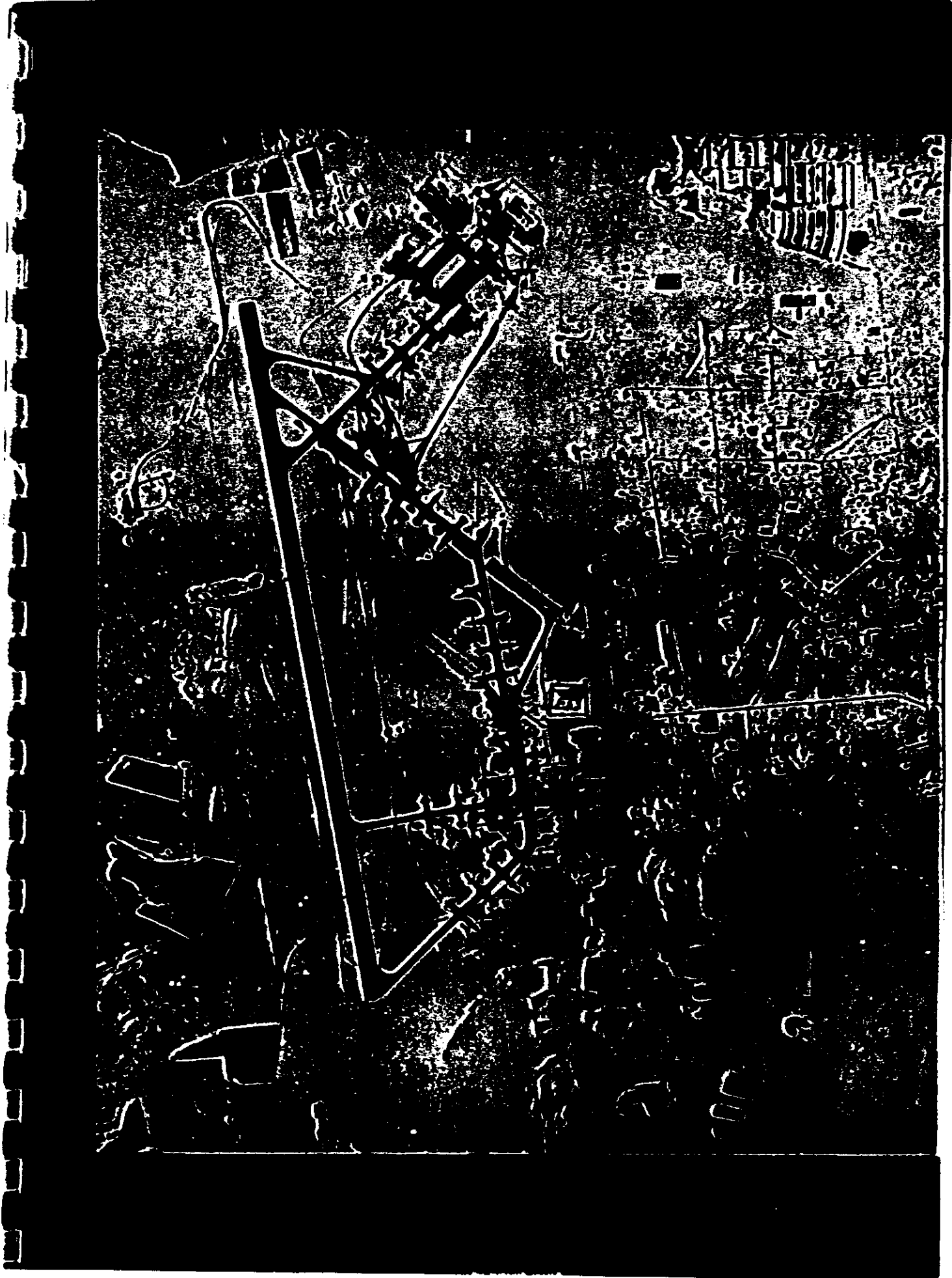
Approximate scan direction
on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.



~~TOP SECRET RUFF~~
NO FOREIGN DISSEM

Handle Via
Talent REFLECT
Control System Only



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Pass 31D FWD
Frame 16
Date of Photography 1 May 1965
Universal Grid Coordinates 27.9 - 12.1
Enlargement Factor 40X
Geographic Coordinates 31-40N 109-43W
Altitude (feet) 604, 385
Camera Attitude:
Pitch 14°51'
Roll 00°03'
Yaw 01°20'
Local Sun Time 1353
Solar Elevation 62°49'
Solar Azimuth 116°
Exposure 1/272 sec

The fwd camera photography appears to be degraded by atmospheric conditions which did not affect the aft camera (See Figure 10) possibly due to the angle of view. The individual bars are distinguishable in Bar Groups 1-3 and the upper section of Group 4. (See the layout drawing, next page, for orientation and identification of the bar groups.)



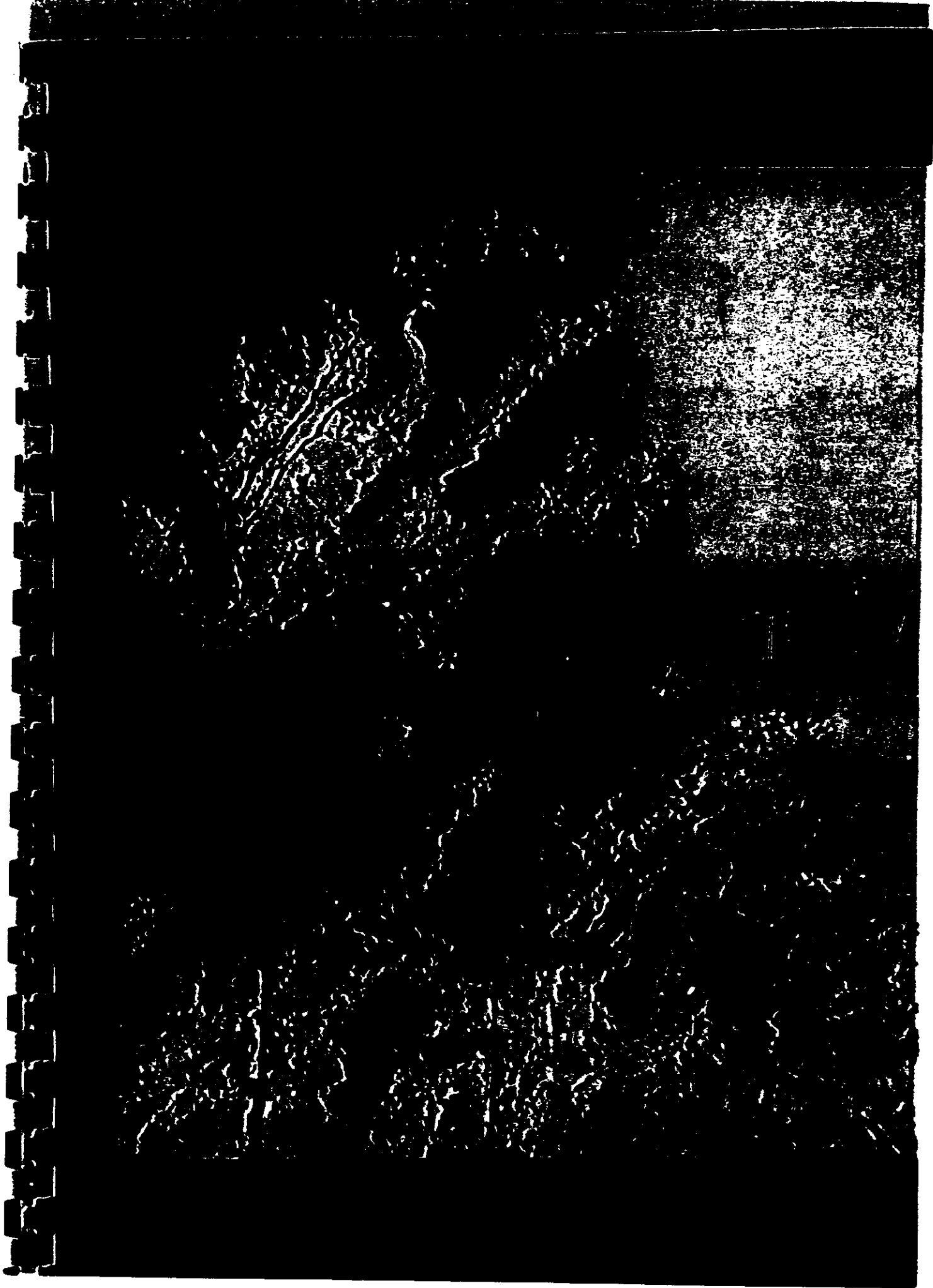
Approximate flight direction on photograph

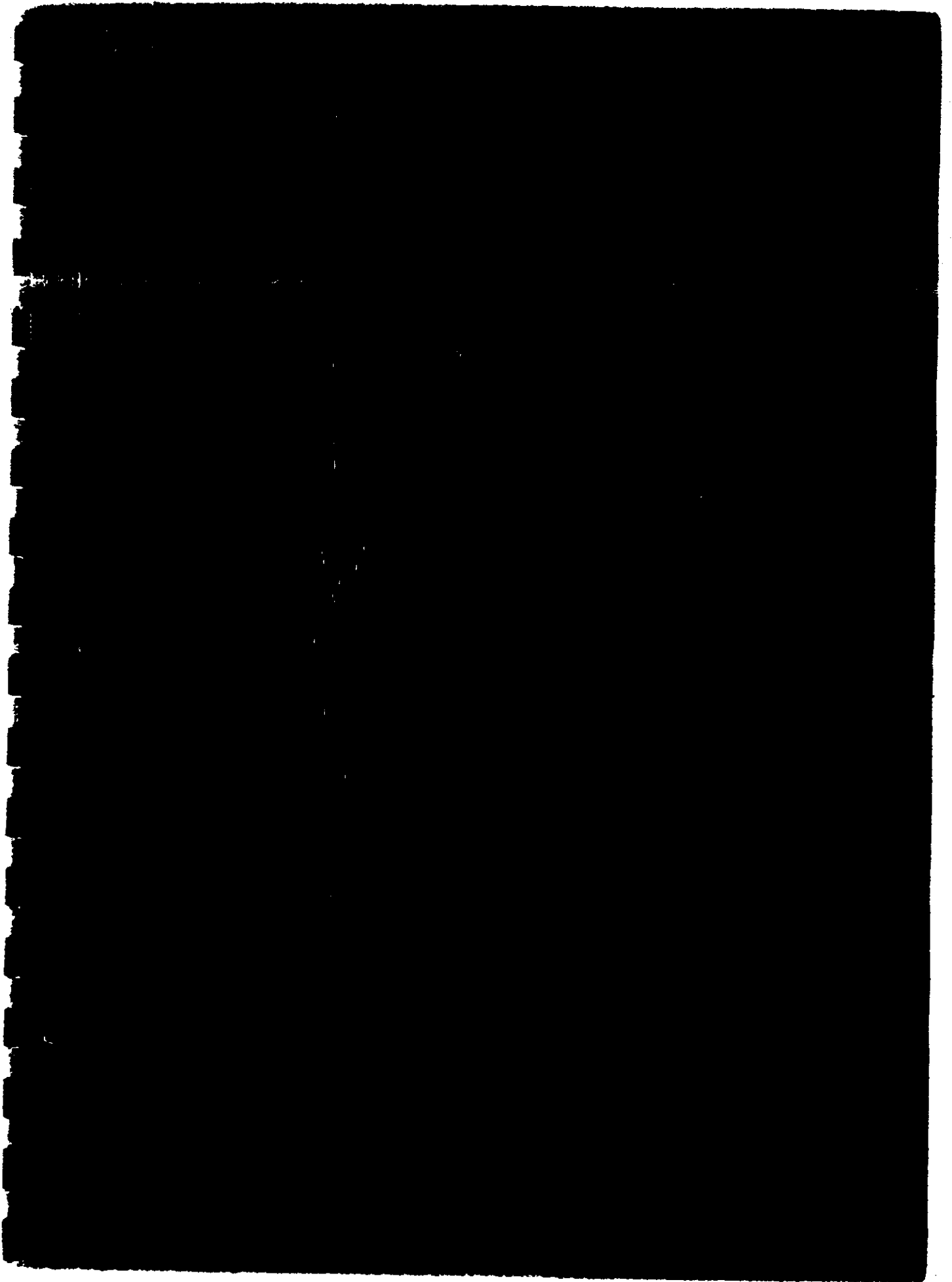


Approximate scan direction on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.







Handle Via
Talent-RTYBOLC
Control System Only

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~



FIGURE 11: FIXED RESOLUTION TARGET, FORT HUACHUCA, ARIZONA
(APT PANORAMIC PHOTOGRAPHY)

NPIC 8 028710/001

- 20K -

~~TOP SECRET RUFF~~

Handle Via
Talent-RTYBOLC
Control System Only

Pass	31D AIT
Frame	21
Date of Photography	1 May 1965
Universal-Grid Coordinates	62.3 - 14.1
Enlargement Factor	40X
Geographic Coordinates	31-43N 109-43W
Altitude (feet)	603, 967
Camera Attitude:	
Pitch	Not Available
Roll	Not Available
Yaw	Not Available
Local Sun Time	1353
Solar Elevation	62°47'
Solar Azimuth	116°
Exposure	1/383 sec

The individual bars are readable in Bar Groups 1-3 only. However, note the chevron-shaped contrast target which was "washed out" in the fwd photography.



Approximate flight direction on photograph



Approximate scan direction on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.



TOP SECRET - RUFF



TOP SECRET - RUFF
NO FORN DISSEM

Handle Via
~~TELINT/RETRO~~
Control System Only

~~TOP SECRET RUFF~~
NO FORN DISSEM



FIGURE 14. FIVEK RESOLUTION TARGET, INDIAN SPRINGS, NEVADA (FAC PANORAMIC PHOTOGRAPHY)

REF ID: A66666

- 27 -

~~TOP SECRET RUFF~~
NO FORN DISSEM

Handle Via
~~TELINT/RETRO~~
Control System Only

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TOP SECRET - RUFF



TOP SECRET - RUFF



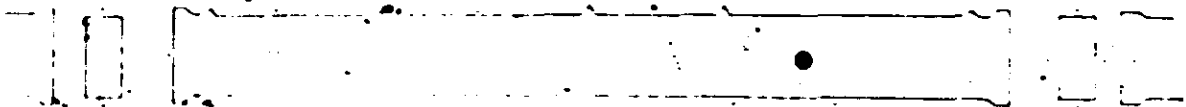
Pass 417 FWD
Frame
Date of Photography 2 May 1964
Universal Grid Coordinates 11.2 - 11.2
Enlargement Factor 40X
Geographic Coordinates 38-40N 117-03W
Altitude (feet) 607.27
Camera Attitude:
Pitch 14° 01'
Roll 00° 08'
Yaw 01° 04'
Local Sun Time 1300
Solar Elevation 71° 37'
Solar Azimuth 145°
Exposure 1/200 sec

Bar Groups 1-9 are distinguishable, but the individual bars are not readable.

Approximate flight direction
on photograph

Approximate scan direction
on photograph

Approximate location of photograph in format. Negative viewed with emission side down



TOP SECRET - RUFF

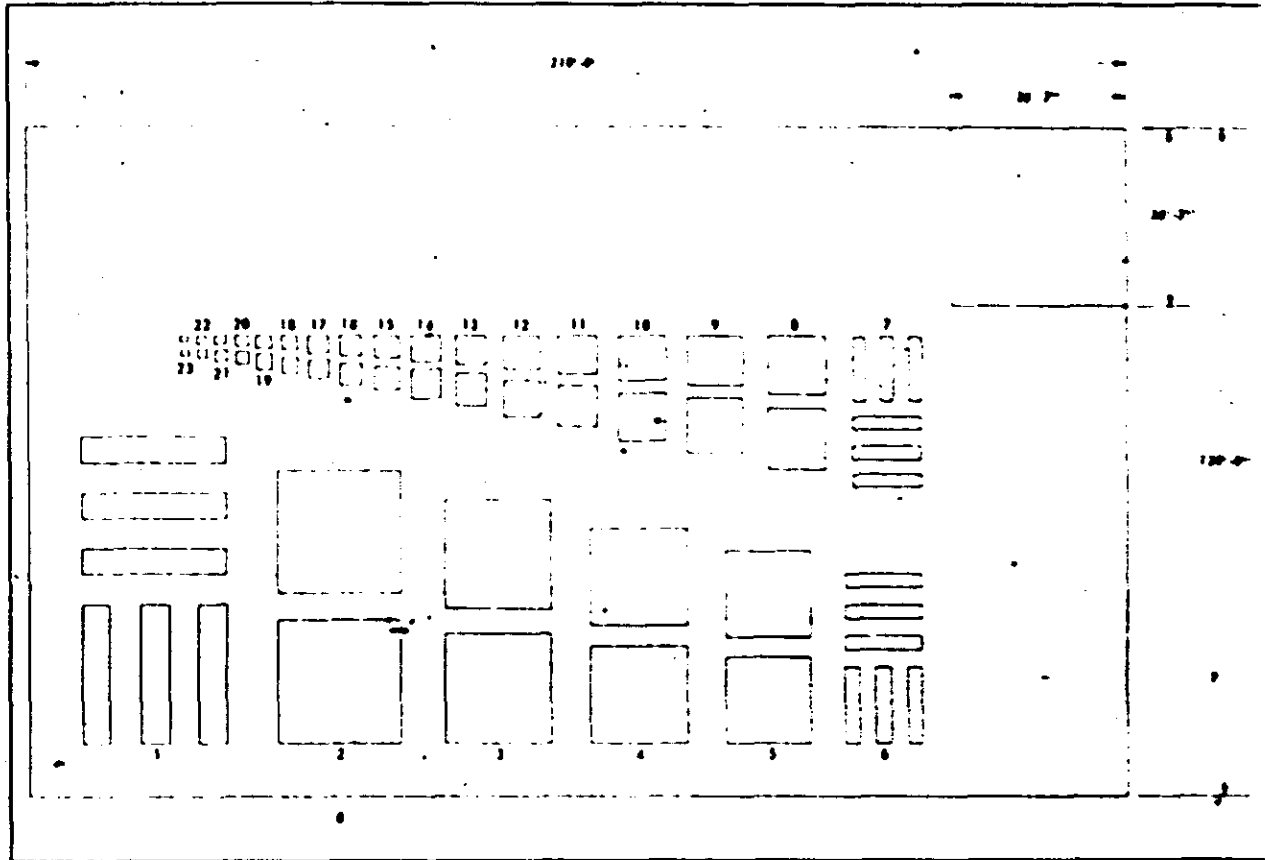


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NO FOREIGN DISSEM

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TAL COTAGE/EMULE
Control System Only



FIGURE 13. INDIAN SPRINGS RESOLUTION TARGET DATA



TARGET BAR WIDTHS

Group	Feet	Inches	Group	Feet	Inches
1	5	7.125	13	1	4.250
2	4	10.000	14	1	2.500
3	4	3.625	15	1	.875
4	3	10.000	16	1	11.500
5	3	5.000	17	0	10.250
6	3	0.500	18	0	0.250
7	2	0.500	19	0	0.125
8	2	7.000	20	0	0.250
9	2	1.875	21	0	6.500
10	1	11.000	22	0	5.750
11	1	0.500	23	0	0.125
12	1	0.250			

Note: The lengths of the bars conform with the aspect ratio as defined by Mil.Std. 150-A: length equals 5 times width.

Handle Via
~~TOP SECRET RUFF~~
Control System Only

~~TOP SECRET RUFF~~
NO FOREIGN DISSEM



FIGURE 14. FIXED RESOLUTION TARGET, INDIAN SPRINGS, NEVADA (AFT PANORAMIC PHOTOGRAPHY)

NPIC N-8048 (10 88)

~~TOP SECRET RUFF~~
NO FOREIGN DISSEM

Handle Via
~~TOP SECRET RUFF~~
Control System Only



Pass	470 AST
Frame	12
Date of Photography	2 May 1955
Universal Grid Coordinates	28.9 - 10.1
Enlargement Factor	40X
Geographic Coordinates	35-35N 114-05W
Altitude (feet)	605, 524
Camera Attitude:	
Pitch	Not Available
Roll	Not Available
Yaw	Not Available
Local Sun Time	1309
Solar Elevation	61°39'
Solar Azimuth	140°
Exposure	1/353 sec

Bar Groups 1-3 can be made out, but individual bars are not readable.

—•— Approximate flight direction on photograph

—•— Approximate scan direction on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.



TOP SECRET - RUFF
NO FORN DISSEM

Handle Via
TALISMANIN
Control System Only



Handle Via
TALISMANIN
Control System Only

TOP SECRET - RUFF
NO FORN DISSEM

Handle Via
~~Talent-RETHOLE~~
Control System Only

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~



FIGURE 15. FIXED RESOLUTION TARGET, PAHRUMP, NEVADA (FWD
PANORAMIC PHOTOGRAPHY)

NPIC K-9047 (10/68)

- 20s -

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~

Handle Via
~~Talent-RETHOLE~~
Control System Only



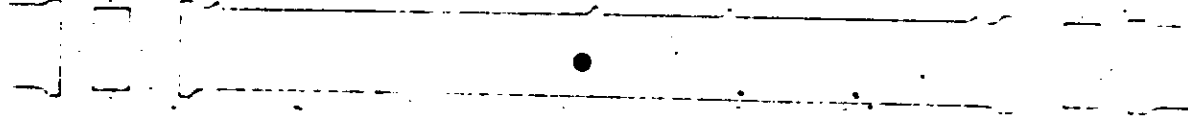
Page 1 of 1
Frame
Date of Photography 2 May 1951
Universal Grid Coordinates 413 101
Enlargement Factor 100
Geographic Coordinates
Altitude (Feet) 6000
Camera Attitude:
Pitch
Roll
Yaw
Local Sun Time 1300
Solar Elevation 61
Solar Azimuth 140
Exposure 1/1000 sec

The individual items are recorded in Form No. 1-44.

Approximate flight direction
on photograph

Approximate scan direction
on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down



TOP SECRET - RUFF

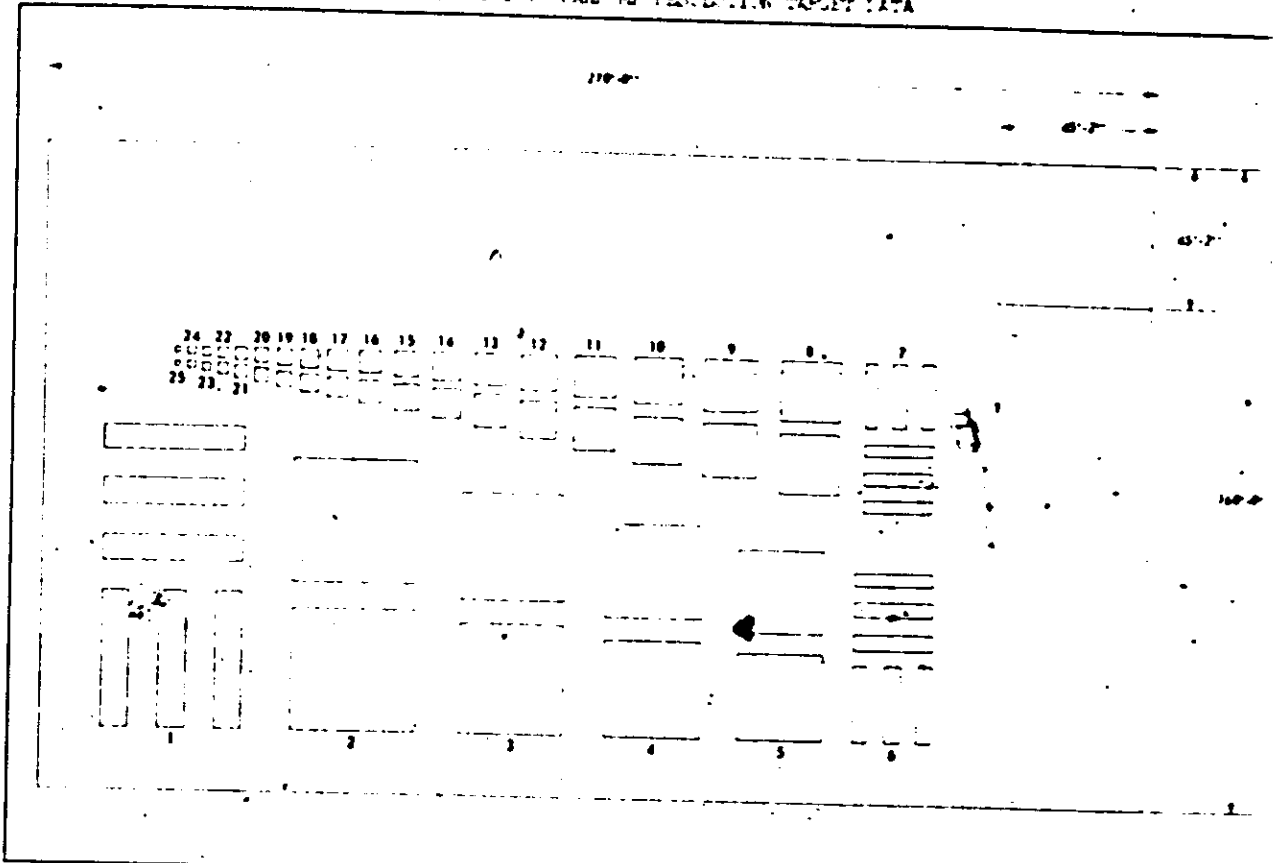
Handle Via
TALENT KEYHOLE
Central System Only



TOP SECRET - RUFF

Handle Via
TALENT KEYHOLE
Central System Only

FIGURE 1. FAIR-WE RESOLUTION TARGET DATA



TARGET BAR WIDTHS

Group	Feet	Inches	Group	Feet	Inches
1	1.000	11.000	14	0.000	0.000
2	0.800	8.800	15	0.000	0.000
3	0.600	6.600	16	0.000	0.000
4	0.500	5.500	17	0.000	0.000
5	0.400	4.400	18	0.000	0.000
6	0.300	3.300	19	0.000	0.000
7	0.250	2.750	20	0.000	0.000
8	0.200	2.200	21	0.000	0.000
9	0.150	1.650	22	0.000	0.000
10	0.125	1.375	23	0.000	0.000
11	0.100	1.100	24	0.000	0.000
12	0.075	0.825			
13	0.050	0.550			

Note: The lengths of the bars conform with the aspect ratio as defined by Mil-Std. 1514A: length equals 4 times width.

Handle Via
~~Teletype~~
Control System Only

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~



FIGURE 17. FIXED RESOLUTION TARGET, PAHRUMP, NEVADA (AFT PANORAMIC PHOTOGRAPHY)

NPIC K-8048 (10-68)

- 204 -

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~

Handle Via
~~Teletype~~
Control System Only



Pass LTD APT
Frame 14
Date of Photography 2 May 1965
Universal Grid Coordinates 44.3 - 11.0
Enlargement Factor 40X
Geographic Coordinates 36-17N 116-04W
Altitude (feet) 606, 393
Camera Attitude:
Pitch Not Available
Roll Not Available
Yaw Not Available
Local Sun Time 1309
Solar Elevation 61°50'
Solar Azimuth 110°
Exposure 1/383 sec

The individual bars are readily distinguished in Bar Group 1 only. They are barely detectable in Groups 2 and 3, and are degraded to a considerable extent.

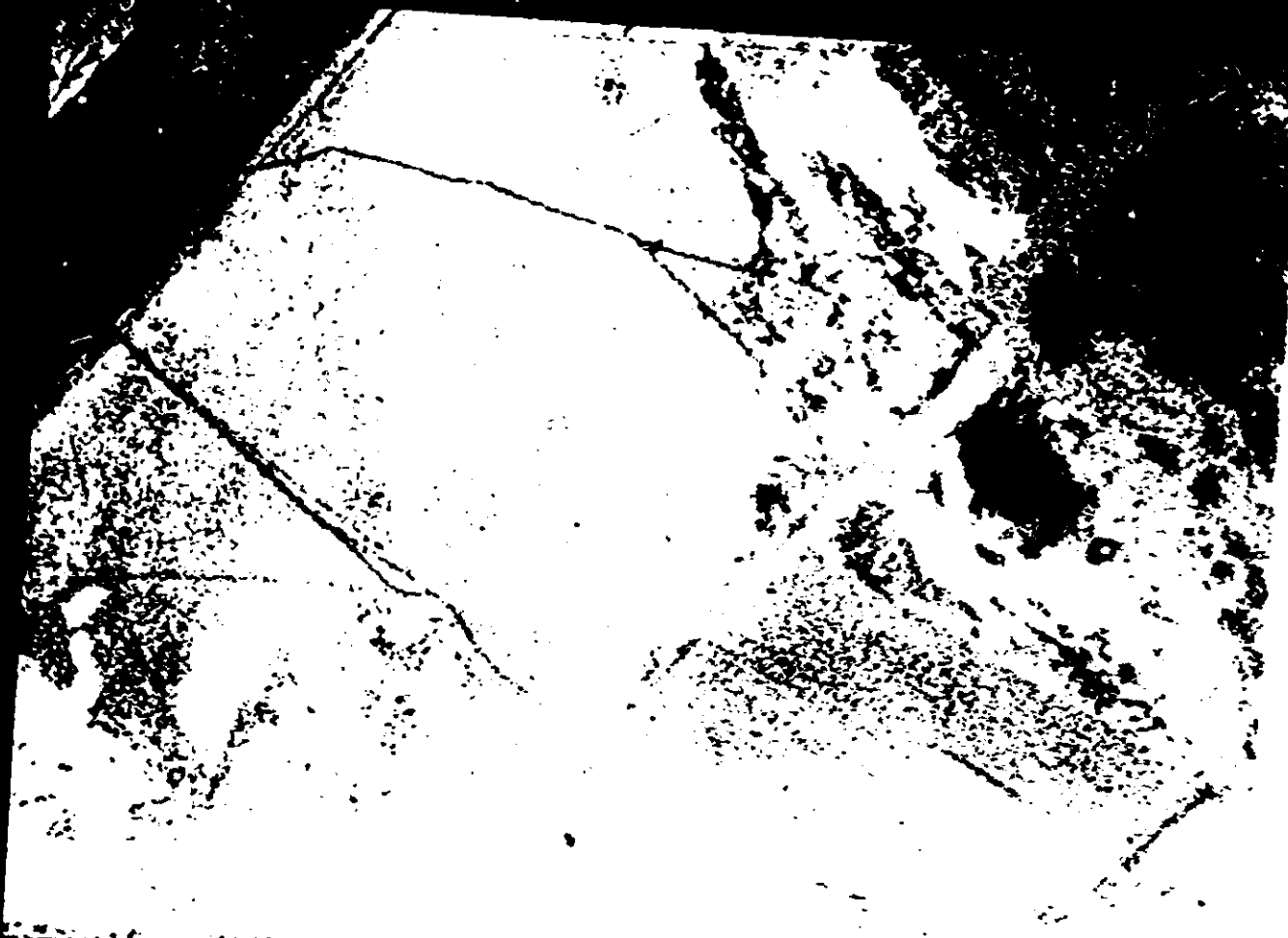
← Approximate flight direction on photograph → Approximate scan direction on photograph

Approximate location of photograph in format. Negative viewed with emulsion side down.



Handle Via
TALCIN-TROVHOLE
Control System Only

TOP SECRET - RUFF
NO FOREIGN DISSEM



TOP SECRET - RUFF
NO FOREIGN DISSEM

Handle Via
TALCIN-TROVHOLE
Control System Only

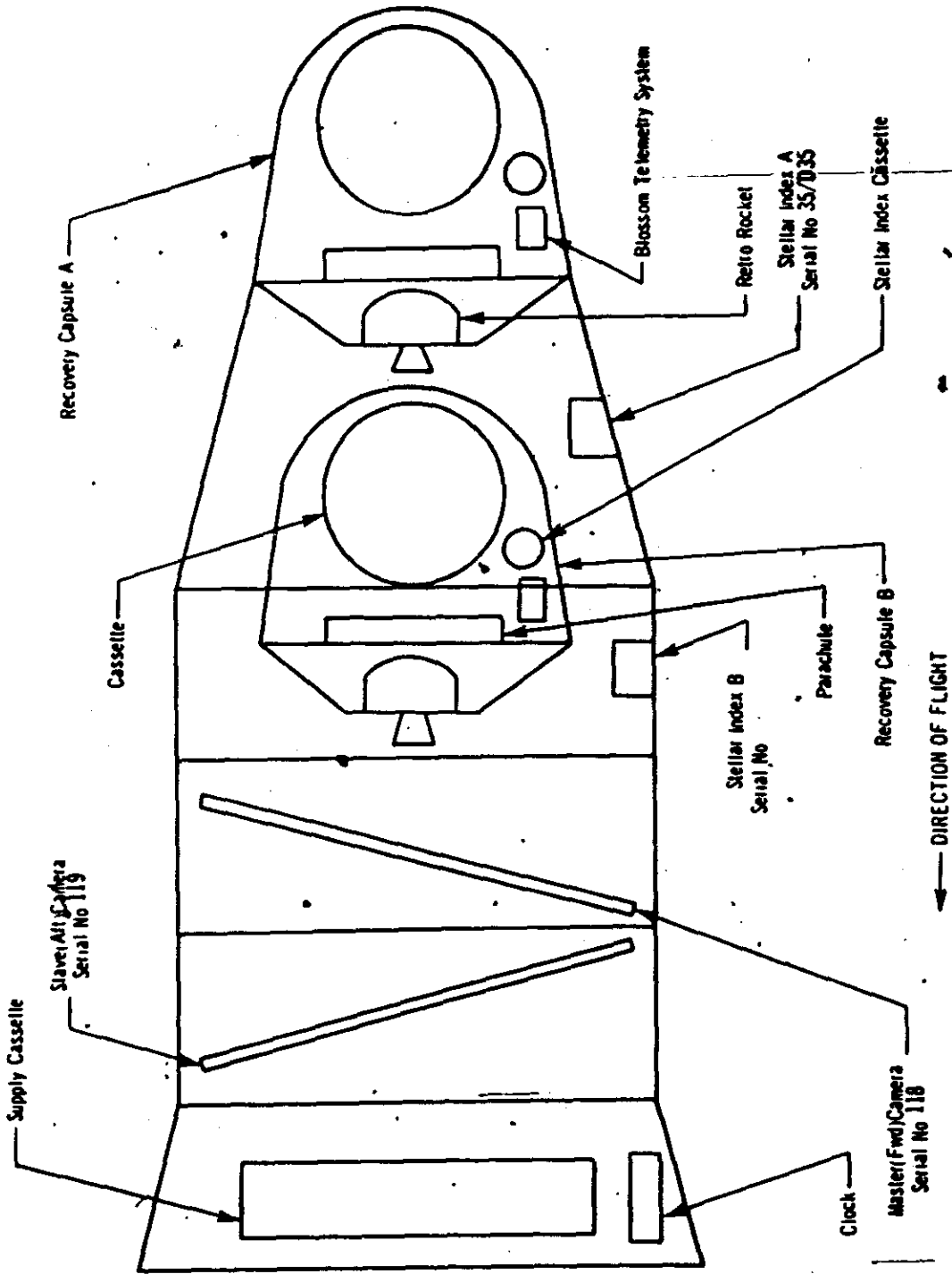
APPENDIX A. SYSTEM SPECIFICATIONS

1. Cameras:

	Master Panoramc	Master Port Horizon	Master Stbd Horizon	Slave Panoramc	Slave Port Horizon	Slave Stbd Horizon	Stellar	Index
Camera No	110	NA	NA	113	NA	NA	35	D35
Lens Serial No	0602435	812313	81203	0572435	815314	813520	10-67	813051
Slit Width	0.250"	NA	NA	0.175"	NA	NA	NA	NA
Aperture	f/3.5	f/6.8	f/8.0	f/3.5	f/6.8	f/8.0	f/1.5	f/4.5
Exposure Time	NA	1/100 sec	1/100 sec	NA	1/100 sec	1/100 sec	2.0 sec	1/500 sec
Filter	Wratten 25	Wratten 25	Wratten 25	Wratten 21	Wratten, 21	Wratten 21	None	Wratten 21
Focal Length (mm)	609.574	54.579	54.920	609.117	54.94	54.70	NA	NA
Film Length (ft)	16,000	NA	NA	16,000	NA	NA	54	40
Splices	4	NA	NA	5	NA	NA	None	None
Emulsion	81-6-1-5	81-6-1-5	81-6-1-5	81-6-1-5	81-6-1-5	81-6-1-5	54-2-1-4	37-1-12-4
Film Type	4404	4404	4404	4404	4404	4404	4401	4400
Res Data, L/mm (A)	*	121	116	*	*	*	*	74
Static Bench Test:								
High Contrast	265	*	*	258	*	*	*	*
Low Contrast	149	*	*	164	*	*	*	*
Dynamic Test:								
I High Contrast	174	*	*	172	*	*	*	*
I Low Contrast	126	*	*	119	*	*	*	*
P High Contrast	179	*	*	186	*	*	*	*
P Low Contrast	112	*	*	114	*	*	*	*

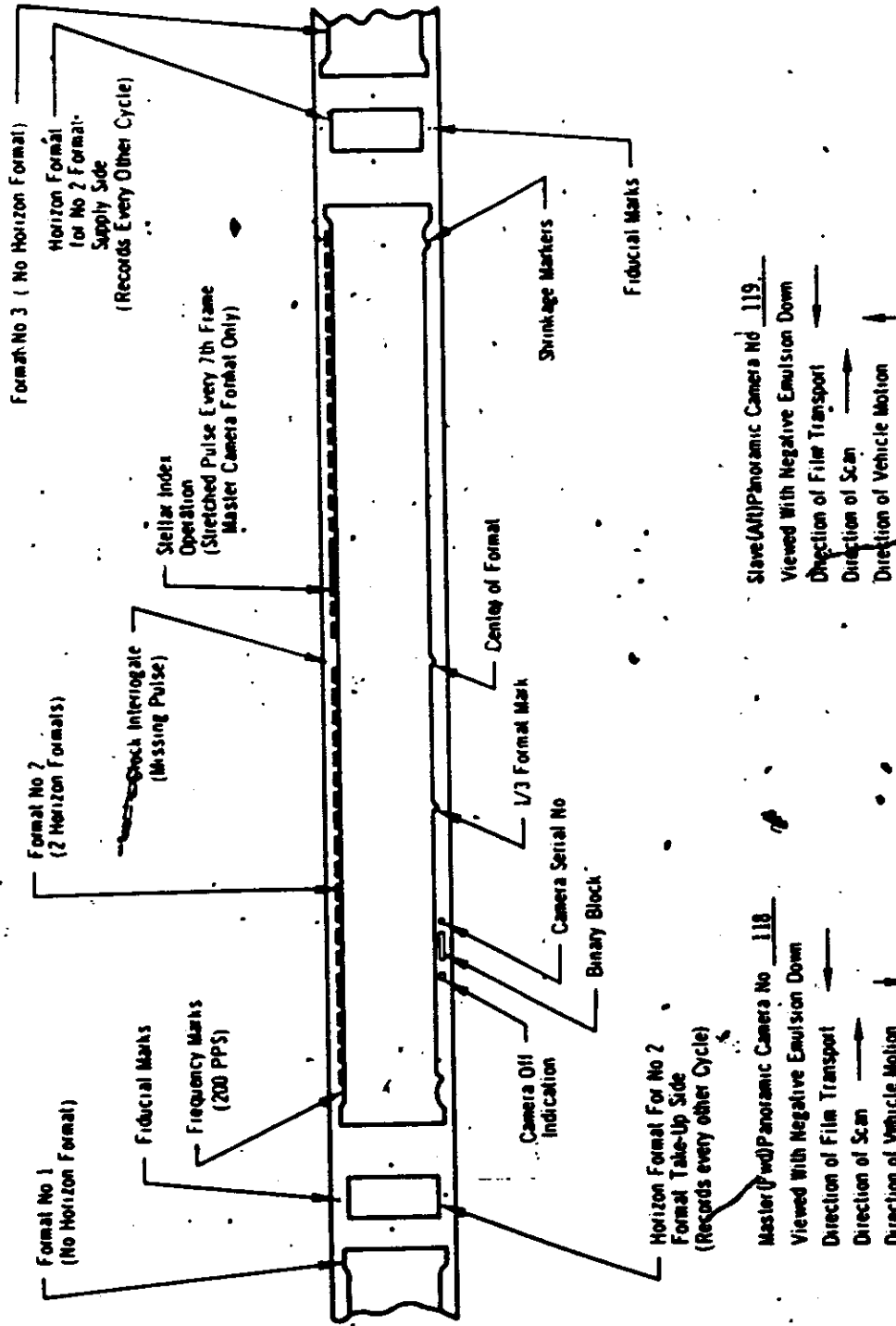
NA - Not Applicable
* - Not Available
A - AMAR

2. VEHICLE CONFIGURATION AND EQUIPMENT LAYOUT



NPIC K-0000 (110/001)

3. PANORAMIC FORMAT CONFIGURATION



NPIC R-909 (110/88)

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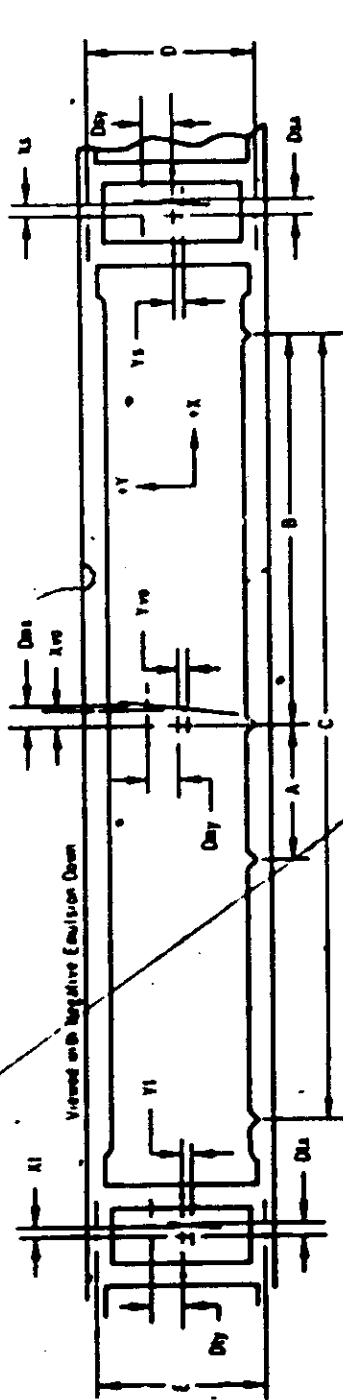
100 CIRCLES

C

THE UNITED STATES OF AMERICA
DEPARTMENT OF JUSTICE
FEDERAL BUREAU OF INVESTIGATION

MEMORANDUM FOR THE DIRECTOR
FROM: SAC, [illegible]
SUBJECT: [illegible]

5. PANORAMIC FORMAT DIMENSIONS



Dimension	Master View Camera 118	Vehicle Motion	Scan Direction	Slave/UD Camera 119	Vehicle Motion	Scan Direction
A	76.1	X1 -0.299	Dx -0.310	A 75.9	X1 -0.160	Dx -0.162
B	354.7	Y1 -0.008	Dy 12.835	B 355.0	Y1 -0.031	Dy 12.462
C	709.2	Xs -0.024	Dxs -0.026	C 709.8	Xs -0.276	Dxs -0.263
D	56.424	Ys -0.055	Dys 12.637	D 56.379	Ys -0.037	Dys 12.103
E	56.422	Xsp +1.339	Dsx +1.360	E 56.424	Xsp -1.089	Dsx -1.072
		Ysp +0.727	Dsy +3.727		Ysp +0.730	Dsy +3.730

Format dimensions

Parameters

Height	55.801
Width	752.1

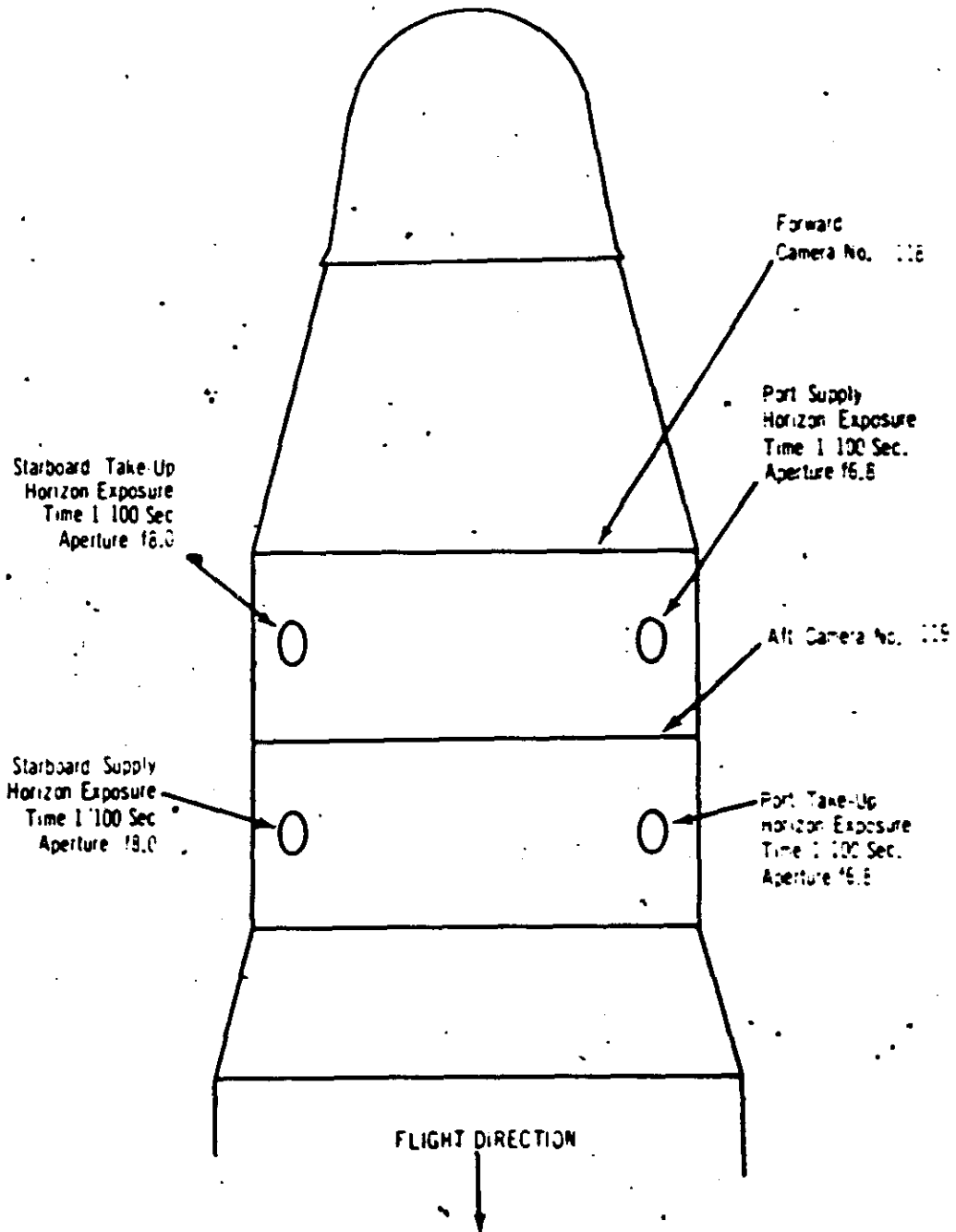
- NOTE:
1. All dimensions are in millimeters and are average dimensions of three formats.
 2. Height of main format is taken at center of format.
 3. Dx, Ds, Dy, X and Y dimensions are taken 18 mm above point defining target center.
 4. Format sign convention:

-X+Y	+X+Y
-X-Y	+X-Y

MPIC K-5083 (10/68)

6. HORIZON LENS SETTINGS

(Viewed from top of vehicle in flight)



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~~NO FOREIGN DISSEM~~

APPENDIX B. DENSITY READINGS

The following Stellar Index density readings were made with a Microphotocopying Densitometer, Model EP 1000, fitted with an ET 20 attachment and an 1.5 millimeter aperture. The readings were obtained at each camera's optical position.

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Handle Via
Talent-KEYHOLE
Control System Only

Handle Via
~~Teletype~~
 Control System Only

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~

Mission 101 1-1

Pass	Frame	STELLAR CAMERA						INDEX CAMERA						
		Dmax	Dmin	Delta	Gross Fog	LIMITING			Dmax	Dmin	Delta	TERRAIN		
						Dmax	Dmin	Delta				Dmax	Dmin	Delta
1D	1	2.05	.29	1.70	.24	.17	1.33	.07	.59	.22	.37			
	2	2.11	.29	1.82	.25	.17	1.25	.07	.52	.36	.16			
	3	2.15	.31	1.84	.26	.95	.75	.67	1.70	.55	.75			
	4	1.96	.32	1.64	.28	.52	1.18	.07	1.70	.52	1.18			
	5	2.25	.36	1.89	.27	.91	.71	.07	1.62	.91	.71			
	6	2.11	.33	1.80	.27	.95	.80	.07	1.16	1.07	.80			
	7	2.11	.33	1.78	.28	.64	1.04	.07	1.47	.68	.59			
	8	2.09	.34	1.76	.30	.32	1.41	.07	1.28	.32	.96			
	9	2.01	.34	1.67	.29	.60	.65	.07	1.55	.90	.65			
	10	1.58	.29	1.29	.23	.27	1.34	.07	1.61	.99	.62			
	11	2.49	.32	2.17	.22	.15	1.52	.07	1.35	.63	.72			
	12	2.51	.37	2.14	.22	.15	2.00	.07	1.67	.43	1.26			
13	1.64	.27	1.37	.22	.75	.70	.07	1.45	.75	.70				
14	2.08	.28	1.80	.22	.61	.70	.07	NR	NR	NR				
15	2.05	.28	1.61	.23	.65	.98	.07	1.63	.72	.91				
16	2.12	.30	1.82	.23	.29	1.06	.07	1.32	.29	1.03				
17	2.01	.27	1.74	.22	.30	1.53	.07	.89	.55	.34				
18	1.99	.28	1.71	.22	.39	1.13	.07	.52	.39	.13				
19	2.31	.32	1.97	.22	.64	1.16	.07	1.80	.64	1.16				
20	2.36	.30	2.00	.22	.41	1.22	.07	.89	.41	.48				
21	2.03	.29	1.74	.22	.65	1.03	.07	.83	.65	.18				
22	2.46	.29	2.15	.22	.29	1.38	.07	NR	NR	NR				
23	2.06	.28	1.78	.22	.85	.68	.07	NR	NR	NR				
24	1.93	.27	1.66	.22	.32	1.41	.07	.94	.32	.62				
25	2.13	.29	1.84	.22	.24	1.37	.07	.90	.24	.76				
26	2.22	.28	1.94	.22	.45	1.26	.07	.85	.45	.40				
27	2.56	.32	2.24	.22	.50	.78	.07	1.30	.56	.74				
28	2.52	.34	2.18	.21	.54	1.33	.07	1.53	.54	.99				
29	2.48	.38	2.10	.22	.64	1.17	.07	.75	.64	.11				
30	2.28	.37	1.91	.22	.43	1.18	.07	.87	.43	.44				
31	2.38	.32	2.06	.22	.55	1.08	.07	.70	.55	.15				
32	2.41	.32	2.09	.22	.32	1.30	.07	.65	.32	.33				
33	2.08	.29	1.79	.22	.32	1.31	.07	1.54	.32	1.22				
34	2.13	.29	1.84	.22	.62	.86	.07	1.40	.62	.78				
35	2.33	.27	2.06	.22	.39	1.49	.07	1.88	.39	1.39				
36	2.13	.27	1.84	.22	.68	.87	.07	1.55	.68	.87				
37	2.13	.27	1.83	.22	.45	.75	.07	1.55	.45	.35				
38	2.11	.28	1.83	.22	.15	1.19	.07	.80	.15	.63				
39	2.26	.29	1.97	.22	.15	1.19	.07	1.08	.15	.63				

NR - Denotes No Reading Made

~~TOP SECRET RUFF~~
~~NO FOREIGN DISSEM~~

Handle Via
~~Teletype~~
 Control System Only

Mission 1019-1

STELLAR CAMERA										INDEX CAMERA				
Page	Frame	Dens	Date	Delta	Gross Fug	LIMITING			TELETYPE					
						Dens	Date	Delta	Dens	Date	Delta			
90	90	2.1	28	.01	.22	.07	.07	0.00	.07	.07	.07	0.00		
91	91	2.2	28	.00	.22	.07	.07	0.00	.07	.07	.07	0.00		
92	92	2.3	28	2.00	.22	.17	.17	1.39	.07	.07	.17	1.39		
93	93	2.4	28	2.16	.22	.15	.15	1.10	.07	.07	.15	1.10		
94	94	2.5	28	1.93	.22	.15	.15	1.24	.07	.07	.15	1.24		
95	95	2.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
96	96	2.7	28	2.07	.22	.15	.15	1.24	.07	.07	.15	1.24		
97	97	2.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
98	98	2.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
99	99	3.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
100	100	3.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
101	101	3.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
102	102	3.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
103	103	3.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
104	104	3.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
105	105	3.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
106	106	3.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
107	107	3.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
108	108	3.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
109	109	4.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
110	110	4.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
111	111	4.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
112	112	4.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
113	113	4.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
114	114	4.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
115	115	4.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
116	116	4.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
117	117	4.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
118	118	4.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
119	119	5.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
120	120	5.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
121	121	5.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
122	122	5.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
123	123	5.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
124	124	5.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
125	125	5.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
126	126	5.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
127	127	5.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
128	128	5.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
129	129	6.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
130	130	6.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
131	131	6.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
132	132	6.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
133	133	6.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
134	134	6.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
135	135	6.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
136	136	6.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
137	137	6.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
138	138	6.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
139	139	7.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
140	140	7.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
141	141	7.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
142	142	7.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
143	143	7.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
144	144	7.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
145	145	7.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
146	146	7.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
147	147	7.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
148	148	7.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
149	149	8.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
150	150	8.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
151	151	8.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
152	152	8.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
153	153	8.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
154	154	8.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
155	155	8.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
156	156	8.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
157	157	8.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
158	158	8.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
159	159	9.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
160	160	9.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
161	161	9.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
162	162	9.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
163	163	9.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
164	164	9.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
165	165	9.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
166	166	9.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
167	167	9.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
168	168	9.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
169	169	10.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
170	170	10.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
171	171	10.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
172	172	10.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
173	173	10.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
174	174	10.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
175	175	10.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
176	176	10.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
177	177	10.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
178	178	10.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
179	179	11.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
180	180	11.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
181	181	11.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
182	182	11.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
183	183	11.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
184	184	11.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
185	185	11.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
186	186	11.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
187	187	11.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
188	188	11.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
189	189	12.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
190	190	12.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
191	191	12.2	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
192	192	12.3	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
193	193	12.4	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
194	194	12.5	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
195	195	12.6	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
196	196	12.7	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
197	197	12.8	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
198	198	12.9	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
199	199	13.0	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		
200	200	13.1	28	1.97	.22	.15	.15	1.24	.07	.07	.15	1.24		

TOP SECRET RUFF
IN FOREIGN DISSEM

Handle Via
 Select-Intervent
 Control System Only

TOP SECRET RUFF

Mission 1017-1

IRAZI CAMBA										
Phase	Frames	Lines	L. D. T. I. N. O.			Gross Fug	Lines	Inch.	Inch.	Inches
			Lines	Inch.	Inches					
101	107	22	0.00	.07	.00	.07	.07	.07	.07	.00
102	107	22	4.00	.07	.00	.07	.07	.07	.07	.00
103	107	27	1.05	.06	.76	.07	.07	.07	.07	.00
104	107	27	2.07	.08	1.11	.07	.07	.07	.07	.00
105	107	28	1.83	.08	.77	.07	.07	.07	.07	.00
106	107	28	.46	.33	1.39	.07	.07	.07	.07	1.05
107	107	33	2.01	.18	1.43	.07	.07	.07	.07	.07
108	107	33	2.18	.19	1.52	.07	.07	.07	.07	.07
109	107	37	1.81	.33	1.11	.07	.07	.07	.07	1.11
110	107	37	1.59	.25	1.33	.07	.07	.07	.07	1.31
111	107	32	1.87	.25	.84	.07	.07	.07	.07	.07
112	107	32	1.56	.24	1.40	.07	.07	.07	.07	.07
113	107	35	2.15	.26	1.15	.07	.07	.07	.07	.07
114	107	34	1.63	.29	1.28	.07	.07	.07	.07	.07
115	107	34	1.66	.31	1.14	.07	.07	.07	.07	.07
116	107	31	2.05	.31	1.14	.07	.07	.07	.07	.07
117	107	26	2.18	.28	.63	.07	.07	.07	.07	.07
118	107	26	1.83	.28	.70	.07	.07	.07	.07	.07
119	107	27	1.71	.27	1.01	.07	.07	.07	.07	.07
120	107	27	2.11	.27	1.01	.07	.07	.07	.07	.07
121	107	27	1.71	.27	1.01	.07	.07	.07	.07	.07
122	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
123	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
124	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
125	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
126	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
127	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
128	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
129	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
130	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
131	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
132	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
133	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
134	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
135	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
136	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
137	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
138	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
139	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
140	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
141	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
142	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
143	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
144	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
145	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
146	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
147	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
148	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
149	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07
150	107	27	1.89	.27	1.01	.07	.07	.07	.07	.07

IRAZI CAMBA

L. D. T. I. N. O.

IRAZI CAMBA

Gross
Fug

Lines

Inch.

Inches

TOP SECRET RUFF

Handle Via
 Select-Intervent
 Control System Only

Mission 1019-1

Pass	STELLAR CAMERA				INDEX CAMERA									
	LUNATING		TERRAIN		LUNATING		TERRAIN							
	Dist	Delta	Dist	Delta	Dist	Delta	Dist	Delta						
230	302	2.20	.27	1.93	.22	.22	1.49	.15	1.34	.07	.07	1.49	.57	.92
	303	.24	.22	.02	.22	.07	.07	.07	.07	.00	.07	.07	.07	.00
	304	.24	.22	.02	.22	.07	.07	.07	.07	.00	.07	.07	.07	.00
	305	.24	.22	.02	.22	.07	.07	.07	.07	.00	.07	.07	.07	.00
	306	2.45	.31	2.12	.24	.24	.75	.22	.53	.07	.07	.75	.23	.22
	312	2.40	.33	2.07	.25	.26	1.47	.31	1.16	.07	.07	.65	.24	.24
	313	2.09	.33	1.76	.26	.26	1.42	.24	1.18	.07	.07	1.42	.24	.24
	315	2.15	.33	1.76	.26	.26	1.42	.24	1.18	.07	.07	1.42	.24	.24
	316	2.36	.37	1.97	.29	.30	1.48	.31	.66	.07	.07	1.48	.31	.66
	317	2.34	.39	1.97	.30	.31	1.44	.37	.66	.07	.07	1.44	.37	.66
	318	2.12	.39	1.97	.31	.32	1.44	.39	.66	.07	.07	1.44	.39	.66
	320	2.09	.37	1.73	.27	.27	1.50	.15	1.32	.07	.07	1.50	.27	.61
	321	2.14	.32	1.81	.25	.25	1.54	.15	1.32	.07	.07	1.54	.27	.61
	326	1.91	.31	1.61	.22	.22	1.61	.92	.66	.07	.07	1.61	.27	.61
	327	1.90	.30	1.60	.22	.22	1.53	.92	.66	.07	.07	1.53	.27	.61
	332	1.84	.28	1.56	.22	.22	1.54	.92	.66	.07	.07	1.54	.27	.61
	333	2.20	.28	1.82	.22	.22	1.67	.92	.66	.07	.07	1.67	.27	.61
	335	2.19	.28	1.81	.22	.22	1.61	.92	.66	.07	.07	1.61	.27	.61
	336	2.13	.29	1.81	.22	.22	1.77	.92	.66	.07	.07	1.77	.27	.61
	342	2.47	.32	2.15	.22	.22	1.82	.92	.66	.07	.07	1.82	.27	.61
	343	.23	.22	.01	.22	.22	.07	.07	.07	.07	.07	.07	.07	.07
	344	2.10	.28	1.82	.22	.22	1.84	.92	.66	.07	.07	1.84	.27	.61
	351	1.95	.26	1.69	.22	.22	1.83	.92	.66	.07	.07	1.83	.27	.61
	352	2.14	.27	1.87	.22	.22	1.86	.92	.66	.07	.07	1.86	.27	.61
	355	2.67	.35	2.32	.23	.23	1.69	.92	.66	.07	.07	1.69	.27	.61
	366	2.29	.39	2.00	.23	.23	1.35	.92	.66	.07	.07	1.35	.27	.61
	374	2.22	.39	1.93	.23	.23	1.35	.92	.66	.07	.07	1.35	.27	.61
	375	1.93	.39	1.69	.23	.23	1.35	.92	.66	.07	.07	1.35	.27	.61
	379	1.78	.35	1.57	.22	.22	1.30	.92	.66	.07	.07	1.30	.27	.61
	380	2.15	.39	1.86	.22	.22	1.42	.92	.66	.07	.07	1.42	.27	.61
	387	2.32	.37	2.05	.22	.22	1.45	.92	.66	.07	.07	1.45	.27	.61
	388	2.23	.36	1.97	.22	.22	1.47	.92	.66	.07	.07	1.47	.27	.61
	389	2.55	.38	2.23	.22	.22	1.35	.92	.66	.07	.07	1.35	.27	.61
	390	2.03	.32	1.80	.22	.22	1.09	.92	.66	.07	.07	1.09	.27	.61
	392	1.88	.33	1.65	.22	.22	1.09	.92	.66	.07	.07	1.09	.27	.61
	393	2.68	.39	2.35	.22	.22	1.67	.92	.66	.07	.07	1.67	.27	.61
780	399	2.20	.29	1.91	.22	.22	1.47	.92	.66	.07	.07	1.47	.27	.61
790	400	2.41	.29	2.12	.22	.22	1.47	.92	.66	.07	.07	1.47	.27	.61
	401	2.43	.32	2.11	.22	.22	1.35	.92	.66	.07	.07	1.35	.27	.61

Average Dist 1.514
Average Delta 0.42
Average Gross Fog 0.07

Dist Range 0.07 - 2.15
Delta Range 0.07 - 1.03
Gross Fog Range 0.07

Average Dist 2.11
Average Delta 0.30
Average Gross Fog 0.24

Dist Range 0.22 - 2.78
Delta Range 0.22 - 0.39
Gross Fog Range 0.22 - 0.33

APPENDIX C. MICRODENSITOMETRY

1. Edge Spread Function:

The technique of obtaining the spread function from microdensitometer edge traces is used as an objective measure of the image quality in mission photography. The spread function curve represents a summation of the separate elements of the photographic system. By taking the Fourier Transform of the spread function the modulation transfer function of the system may be obtained.

To satisfy the desire to express image quality in terms of a value, a single number is determined from the spread function curve by measuring its width at 50 percent amplitude. This width is expressed as a micron distance in image space and may be converted to a distance on the ground. On domestic passes, where 3-bar resolution targets have been available the ground distance determined from edge trace analysis and from the targets has been found to be comparable.

The microdensitometric analysis of edges in the image requires that the object edge fulfill the conditions of a unit step function, i.e., exist for an appreciable distance at a fixed brightness level and change abruptly to a new level which exists for an appreciable distance. This requirement is usually achieved by rooftops of buildings in large-scale photography, and aircraft runways or taxiways in small-scale photography.

The mission is examined to determine the MIP frame (Mission Information Potential), which is a subjective selection of the best photography. Straight edges in this imagery meeting the criteria of a step function for a length of at least 120 microns are selected for scanning with the microdensitometer.

The microdensitometer used for the traces in this report is located at an Air Force facility. The location of the traces was directed by representatives from NPIC with the Air Force. The instrument is the Minolta Micro-Analyzer used with an effective slit of 1 micron by 50 microns. A scan speed of 0.05 millimeter/minute and a chart speed of 4 inches/minute was used for a recording to specimen expansion of 2032:1. One inch on the recording equals 12.5 microns on the specimen. The traces produced represent a

plot of deflection versus distance. The deflection of the pen is essentially linear with density and the horizontal lines on the chart numbered 1 to 7 equal 0 to 3.0 density.

At the same time the traces were made, the electronic output signals from the instrument were digitized as density values and recorded on paper tape for direct analysis by an IBM 1710 computer. Three outputs from the computer are shown in the Summary Table of Edge Traces on page 36: the width of the Line Spread Function at 50 percent maximum amplitude, the MTF/AIM intersect point, and the Machine RES. The procedure involved in the derivation of these values in the IBM 1710 computer is described in the Air Force Technical Report No 101-31 (Page 79-82). The following table is a summary of the determinations made from edge traces of the original negative. The imagery traced is contained in the frame considered to be typical of the best in this mission.

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FIGURE 18. TARGETS, MICRODENSITOMETRIC TRACES NOS 1-6

NPIC K-8084 (10 68)

- 35a -

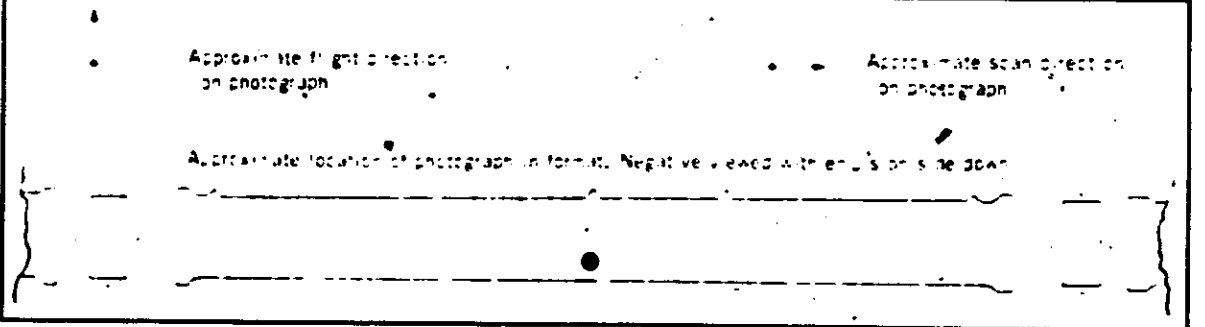
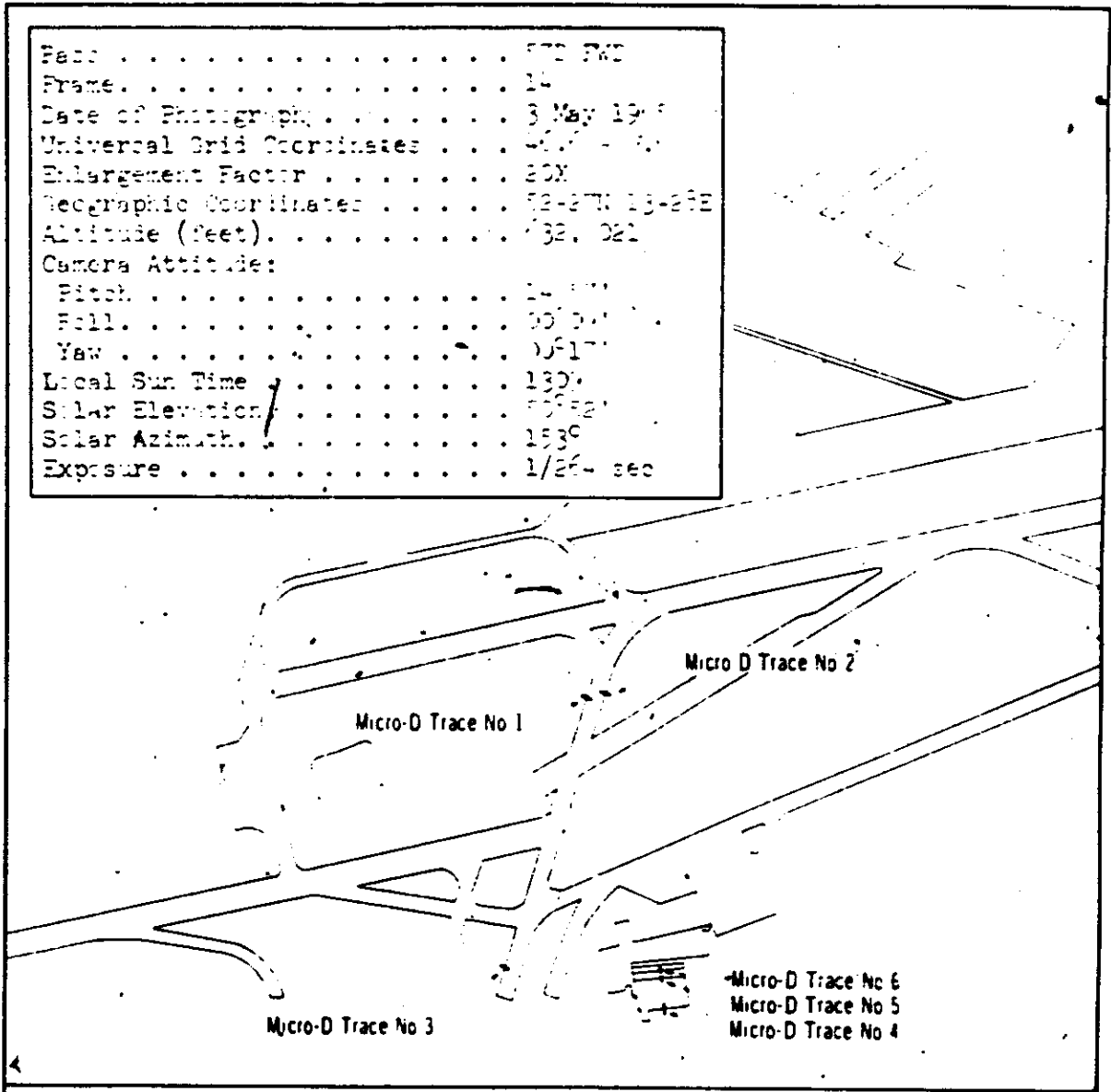
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Roll	570 FWD
Frame	14
Date of Photograph	3 May 1948
Universal Grid Coordinates	41 7 1 10
Enlargement Factor	20X
Geographic Coordinates	52-27N 13-28E
Altitude (feet)	732, 021
Camera Attitude:	
Pitch	14-17°
Roll	90-91°
Yaw	0-17°
Local Sun Time	130°
Solar Elevation	50-52°
Solar Azimuth	153°
Exposure	1/250 sec



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FACTS - 100000
Central System - 100000



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FACTS - 100000
Central System - 100000

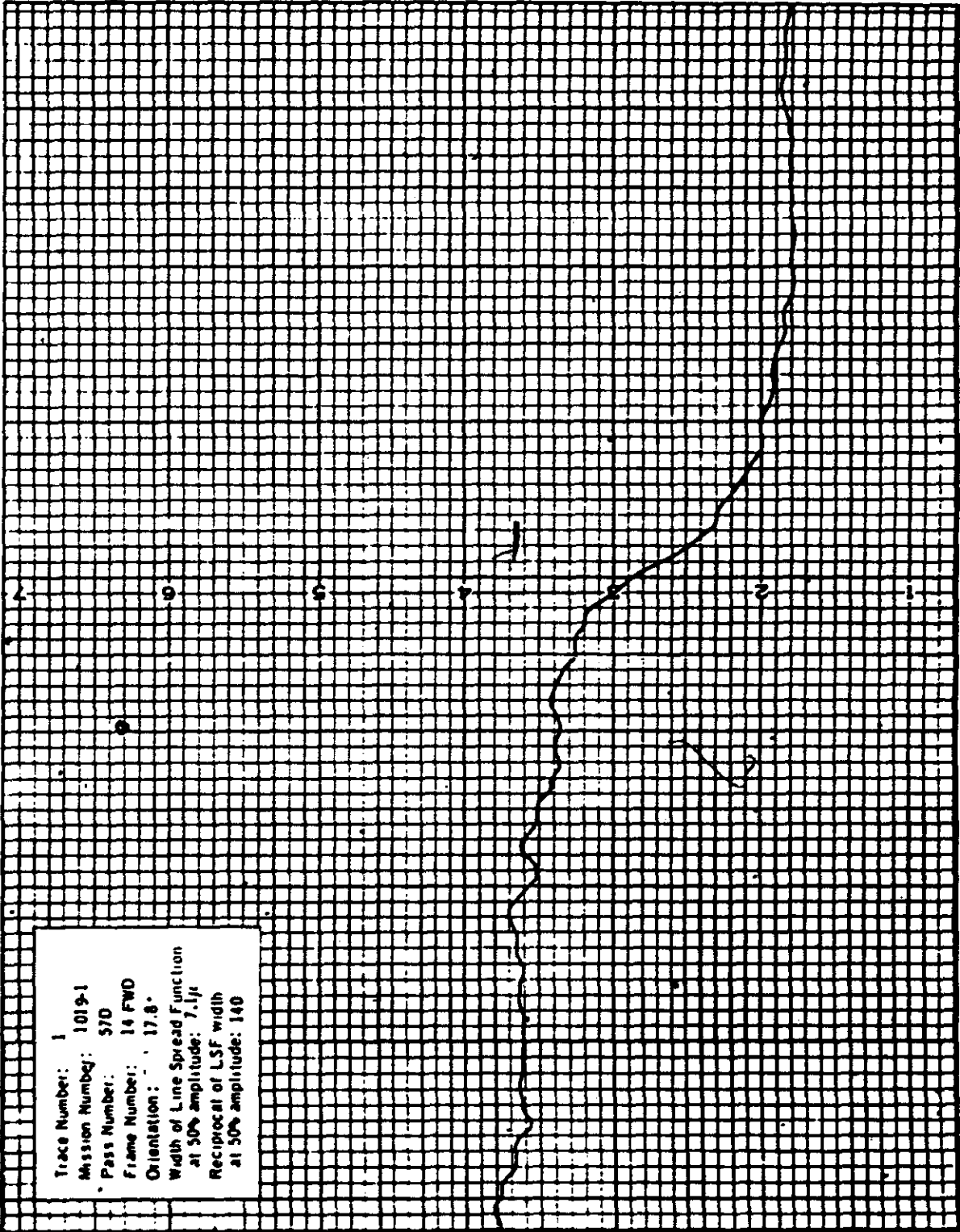
SUMMARY TABLE OF EDGE TRACES
Mission 1019-1

Trace Number	Pass/Trace	LINE BEHEAD/UNION		MTR/IDU Interest	Edge Orientation
		50% Width	100% Width		
1	5TP/2AT	11.1	149	80	17.8°
2	5TP/2AT	8.6	117	79	17.8°
3	5TP/2AT	8.8	113	81	17.8°
4	5TP/2AT	10.8	93	65	94.6°
5	5TP/2AT	10.8	113	57	94.6°
6	5TP/2AT	11.1	85	64	94.6°





MICRODENSITOMETRIC TRACE

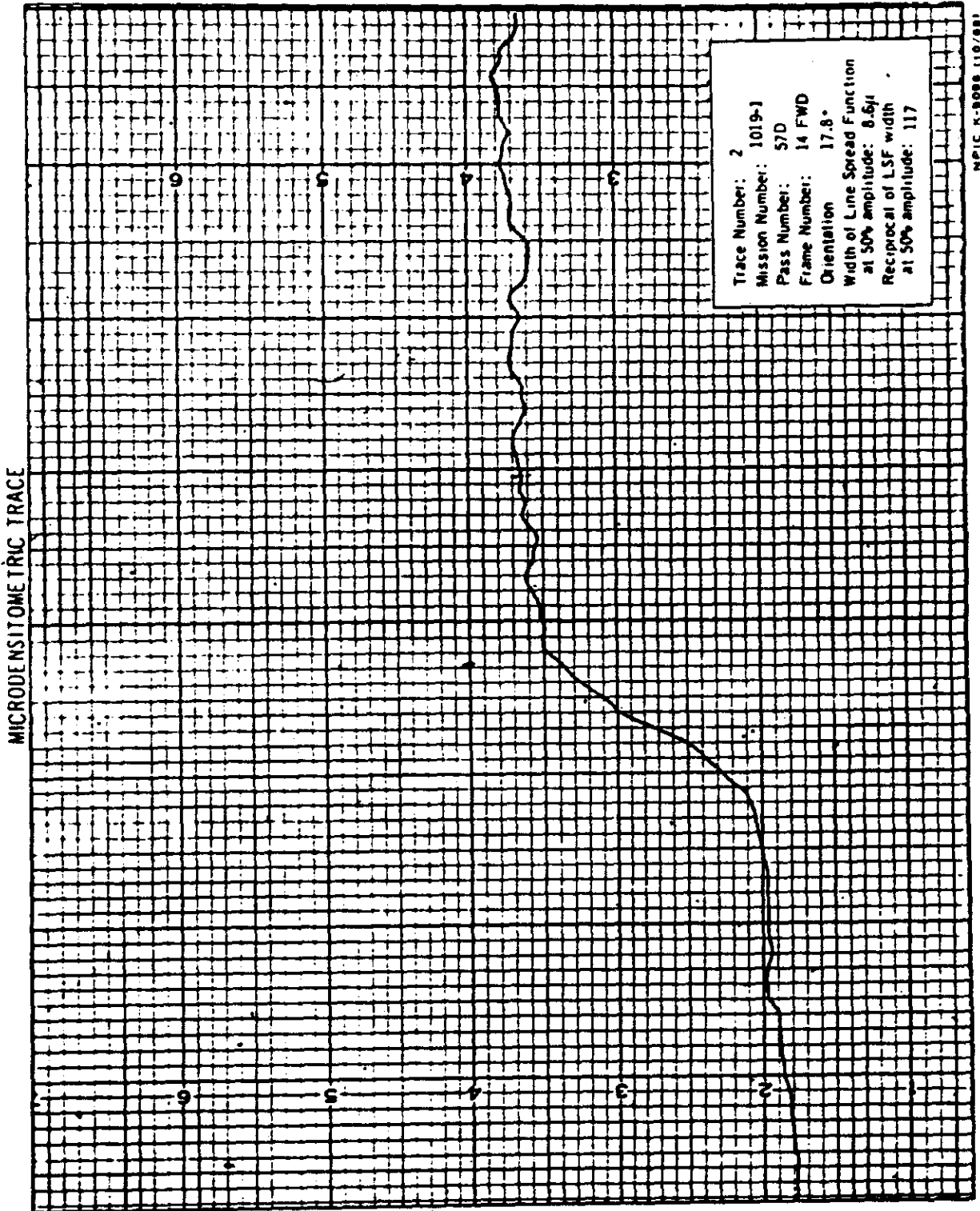


MPIC K-9088 (19/08)

Trace Number: 1
Mission Number: 1019-1
Pass Number: 570
Frame Number: 14 FWD
Orientation: 17.8°
Width of Line Spread Function
at 50% amplitude: 7.1/c
Reciprocal of LSF width
at 50% amplitude: 140

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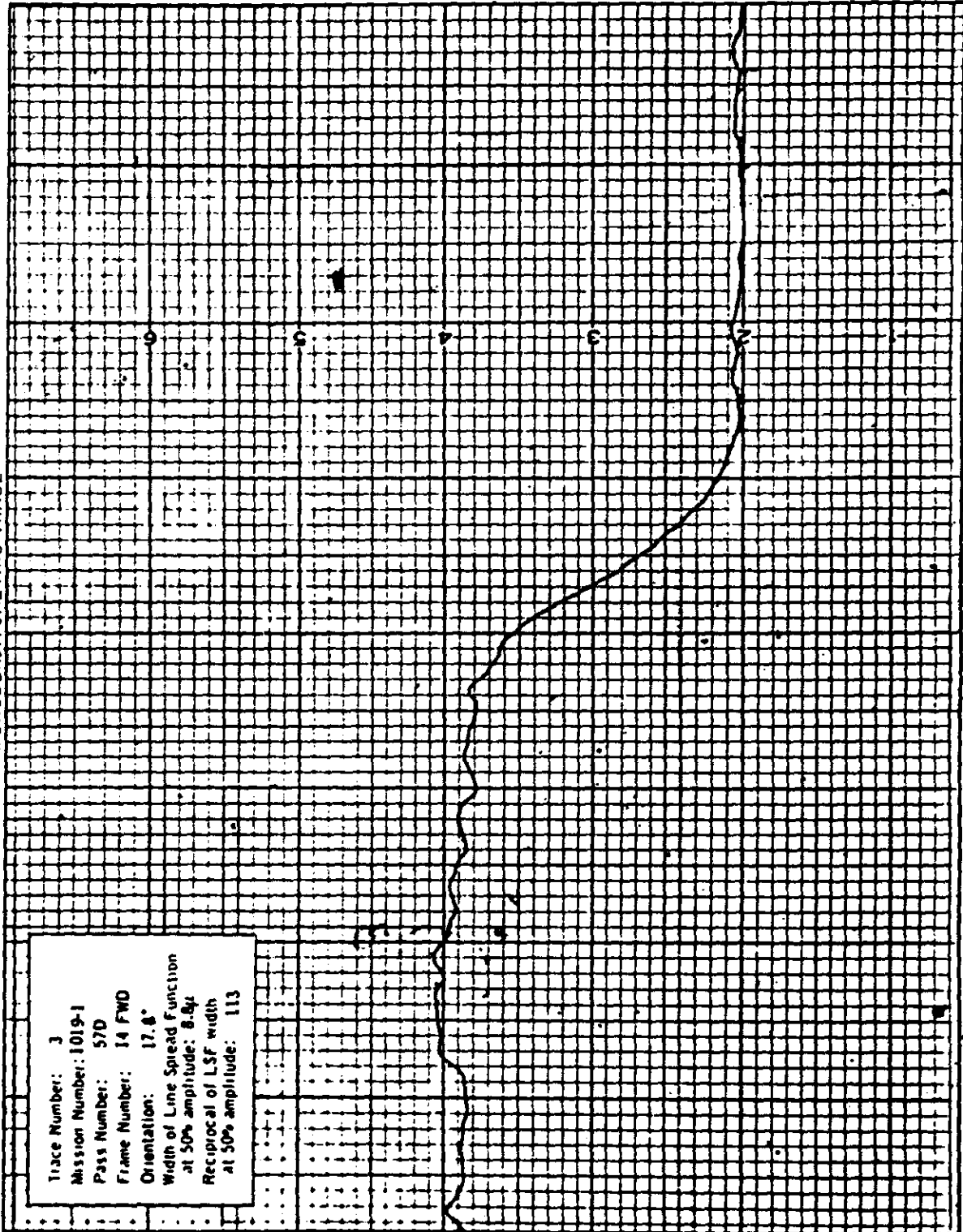
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MICRODENSITOMETRIC TRACE



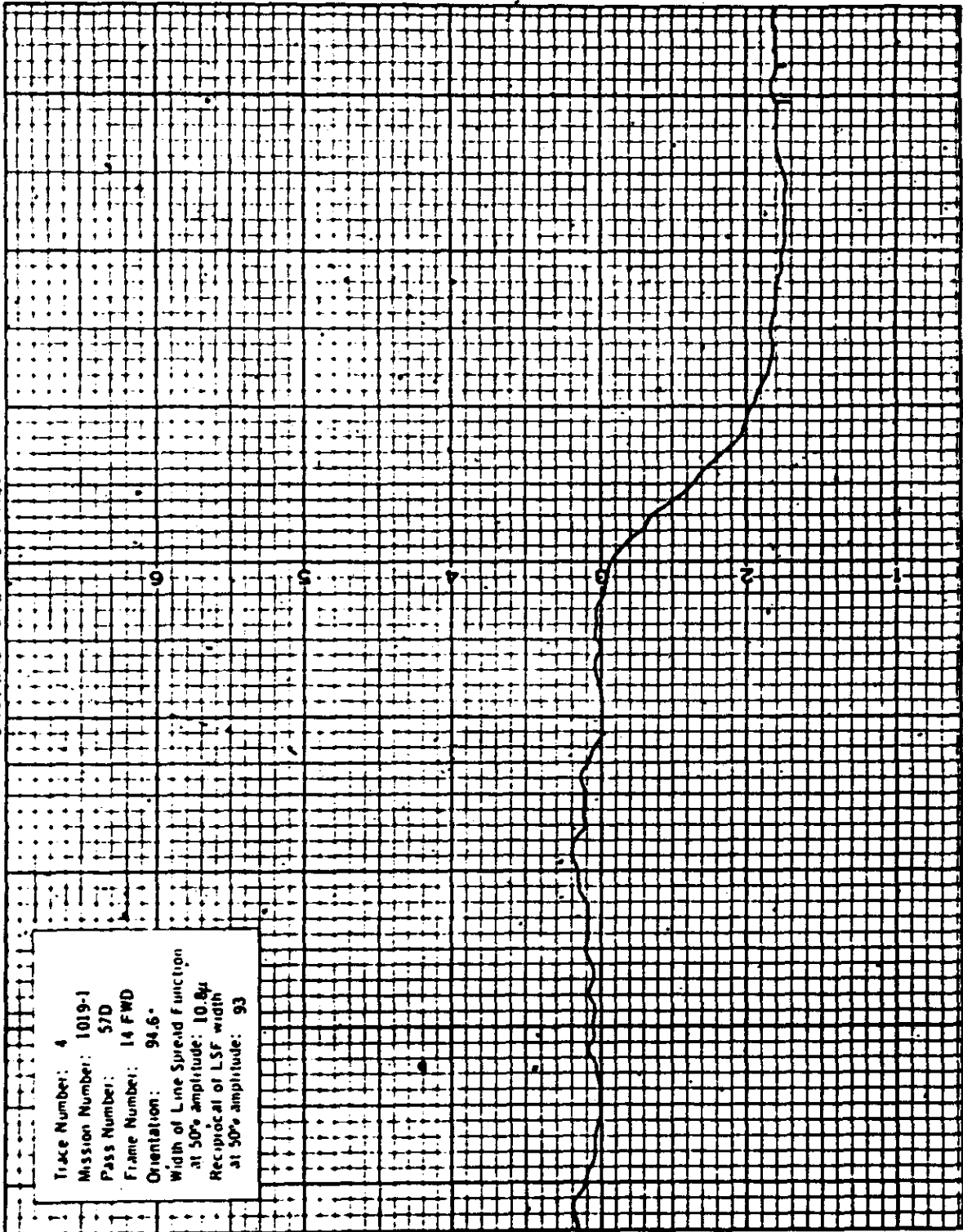
NPIC N-8087 (10/88)

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Talent-~~NETWOL~~
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-NO FOREIGN DISSEM-



MICRODENSITOMETRIC TRACE

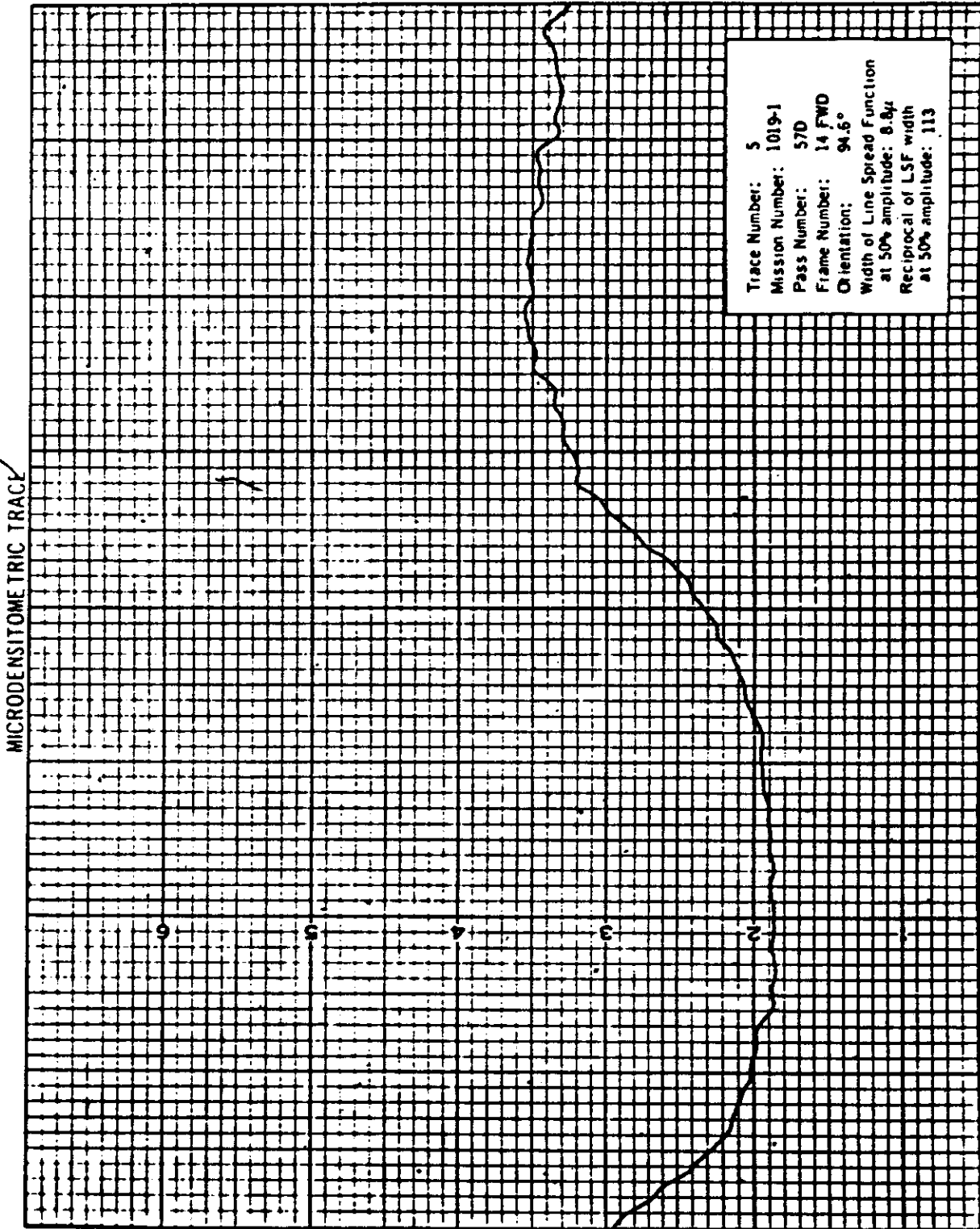


NPIC K-8088 (10/88)

Trace Number: 4
Mission Number: 1019-1
Pass Number: 57D
Frame Number: 14 FWD
Orientation: 94.6°
Width of Line Spread Function
at 50% amplitude: 10.8μ
Reciprocal of LSF width
at 50% amplitude: 93

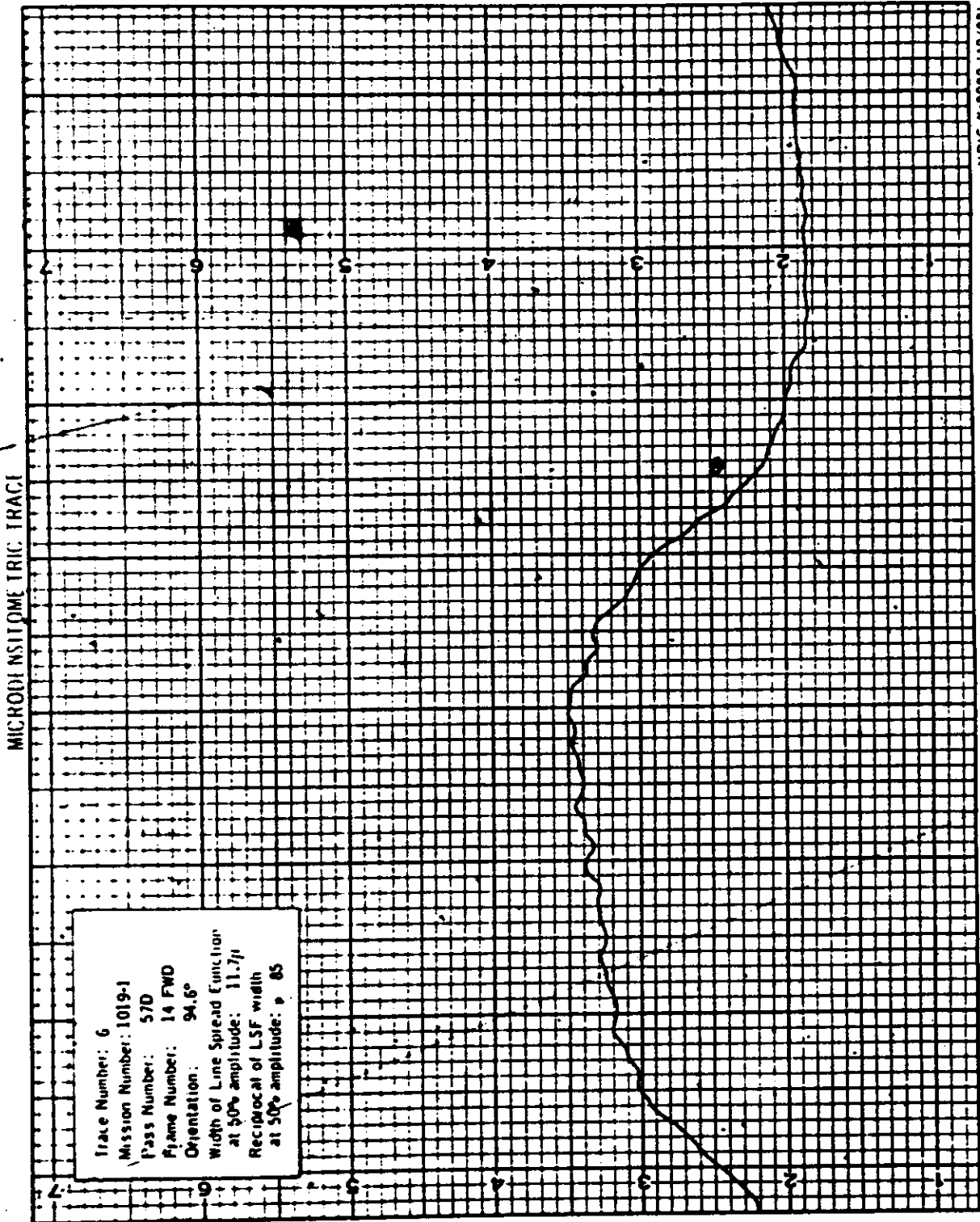
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Handle Via
~~Talent KEYHOLE~~
Control System Only

~~TOP SECRET RUFF~~
NO FOREIGN DISSEM



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Handle Via
~~Talent KEYHOLE~~
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APPENDIX B, CLOUD COVER ANALYSIS

1. Introduction:

This study represents a statistical analysis of the cloud cover on the photography of Mission 1019-1. The basis of this study is the cloud cover data for each quarter segment of every individual frame of photography. The data is obtained by analysts specifically trained in estimating cloud cover by designated categories.

Five cloud categories have been formulated for use in this photography (Reference, Table 1). These categories allow for the wide latitude of cloud cover conditions commonly found on a frame of this photography. Note in Table 1 that a mean cloud percentage value has been calculated for each category for use in determining a combined cloud cover percentage for all operational passes of the mission.

The occurrence of each cloud category within an operational pass is expressed as a percentage of 100 and appears in Table 2. Each percentage is a ratio of the number of occurrences of a given cloud cover category to the total number of cloud observations in a photo pass. For example: if the number of category 2 occurrences in a given pass is 200 out of a total of 1000 (250 frames x 4 quarters) all categories combined, then 20 percent of the pass would be classified as category 1.

Also a cloud cover percentage per pass is included in the last column of Table 2 under "cloud cover % per pass". This value is determined by the summation of the products of category percentage in each pass and the mean cloud percentage for that category as established in Table 1. For example: if it is determined that the following percentages exist in a given pass:

20% Category 1
15% Category 2
30% Category 3
25% Category 4
10% Category 5

Then, by using the mean cloud percentage established in Table 1 the following computations are made:

0.20 x 5.0	=	1.00%
0.15 x 17.5	=	2.63%
0.30 x 38.0	=	11.40%
0.25 x 75.0	=	18.75%
0.10 x 100.0	=	10.00%
		<u>43.78%</u>

Hence, 43.8 percent of this pass is cloud covered.

TABLE 1

CLOUD COVER CATEGORIES

CATEGORY NUMBER	PERCENT OF CLOUD COVER	DESCRIPTION	MEAN CLOUD PERCENTAGE
1	Less than 10%	Clear	5%
2	10% - 25%	Small Scattered Clouds*	17.5%
3	26% - 50%	Large Scattered Clouds	38%
4	51% - 99%	Broken or Connected Clouds	75%
5	100%	Complete Overcast	100%

Cloud Cover Data, Mission 1019-1
 PERCENTAGE OF CLOUD COVER CATEGORIES BY PASS

Pass Number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	Cloud Cover % Per Pass	Pass Number	1	2	3	4	5	Cloud Cover % Per Pass
20	83.1	2.4	8.1	6.4	0.0																300	48.5	6.5	4.5	30.0	10.5	19.7	
30	31.0	2.6	9.6	48.7	6.1																400	0.4	0.6	32.3	64.0	2.7	49.3	
40	72.4	5.8	11.0	5.5	3.3																500	25.0	24.5	36.1	14.1	0.0	83.2	
50	43.9	19.1	11.0	17.2	18.8																600	80.3	10.6	6.1	3.0	0.0	40.1	
60	27.2	10.2	12.4	17.9	3.3																700	57.7	12.5	17.0	10.8	0.0	19.7	
70	41.1	12.1	8.2	20.7	17.9																800	96.9	2.6	0.5	0.0	0.0	5.5	
80	9.0	7.3	20.1	57.8	5.8																900	39.8	9.3	2.8	48.1	0.0	49.8	
90	41.7	1.6	15.8	44.6	23.6																1000	43.8	7.3	13.5	28.6	6.8	36.9	
100	78.6	14.3	7.1	11.5	19.5																1100	46.7	2.2	11.1	37.4	0.6	31.1	
110	67.1	3.5	12.0	17.4	0.0																1200	63.9	10.2	8.0	17.6	0.3	21.3	
120	11.6	13.4	18.7	49.1	14.2																1300	100.0	0.0	0.0	0.0	0.0	5.0	
130	28.8	12.2	18.3	25.4	17.3																1400	49.0	5.6	2.6	38.6	4.2	37.6	
140	55.4	16.9	14.7	12.6	0.4																1500	52.6	12.5	18.4	16.5	0.0	24.2	
150	54.2	6.6	6.2	19.8	13.2																1600	87.3	4.6	6.2	1.9	0.0	9.0	
160	1.7	1.1	26.1	71.1	0.0																1700	42.6	16.5	17.0	23.3	0.6	24.5	
170	100.0	0.0	0.0	0.0	0.0																1800	26.9	16.7	19.9	33.3	1.2	20.1	
180	70.0	0.0	4.5	58.0	37.5																1900	42.7	9.7	13.3	27.6	6.7	36.3	
190	34.4	38.5	24.0	3.1	0.0																2000	42.7	9.7	13.3	27.6	6.7	36.3	

Average percentage by category for mission:
 Overall mission cloud cover percentage:

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APPENDIX E. MISSION COVERAGE STATISTICS

Summary of Plottable Photographic Coverage, Mission 1019-1

Country	FORWARD CAMERA		AFT CAMERA		TOTALS	
	Linear m	Square m	Linear m	Square m	Linear m	Square m
USSR	13,010	1,908,182	12,697	1,866,228	25,707	3,774,410
China	1,371	193,530	2,283	322,162	3,654	515,692
Greenland	754	120,324	796	121,866	1,550	242,190
India	710	70,359	702	77,199	1,412	147,558
Mexico	595	76,720	565	71,960	1,160	148,680
Burma	443	56,840	380	51,940	823	108,780
Indonesia	328	23,628	308	22,080	636	45,708
Mauritania	320	44,800	364	50,960	684	95,760
Saudi Arabia	308	43,120	390	54,600	698	97,720
Poland	268	41,200	269	42,424	537	83,624
Uruguay	236	30,388	294	38,842	530	69,230
Angola	235	17,766	223	16,821	458	34,587
Rumania	211	401,698	221	33,150	432	64,848
Mongolia	193	30,108	183	28,326	376	58,434
Paraguay	174	34,452	99	13,860	273	48,312
Iran	166	20,588	175	24,500	341	45,088
Czechoslovakia	164	25,584	162	25,272	326	50,856
East Germany	164	25,584	158	24,648	322	50,232
Brazil	155	24,810	229	34,060	384	58,870
Pakistan	145	20,830	128	18,012	273	38,842
Argentina	143	7,932	47	3,924	190	11,856
Senegal	107	14,980	74	10,360	181	25,340
Bulgaria	103	13,392	130	16,848	233	30,240
Finland	101	13,448	240	36,572	341	50,020
Southwest Africa	101	6,560	25	1,890	126	9,450
South Korea	86	1,296	62	852	148	2,148
Hungary	84	13,104	68	10,608	152	23,712
North Vietnam	64	8,960	25	3,300	89	12,460
Turkey	62	5,328	14	1,008	76	6,336
Afghanistan	58	8,390	93	13,112	151	21,502
Kashmir	53	17,950	64	9,216	117	17,166
Maldives	53	7,420	37	5,180	90	12,600
Spanish Sahara	53	7,420	70	9,800	123	17,220

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APPENDIX E. MISSION COVERAGE STATISTICS

Summary of Plottable Photographic Coverage, Mission 1019-1 (Cont'd)

Country	FORWARD CAMERA		AFT CAMERA		TOTALS	
	Linear in	Square in	Linear in	Square in	Linear in	Square in
Taiwan	52	1,400	62	840	114	2,240
Austria	41	6,396			41	6,396
France	41	1,752			41	1,752
West Germany	41	6,396	54	8,424	95	14,820
North Korea	37	2,160	123	10,656	160	12,816
Japan	21	300	10	150	31	450
Canada	14	192	159	23,610	173	23,802
Portugal	8	141	37	564	45	705
Thailand	8	1,120	10	1,400	18	2,520
Denmark			43	3,520	43	3,520
Sweden			76	2,080	76	2,080
TOTAL	21,281	2,980,548	22,149	3,111,024	43,430	6,091,572
Continental US	1,178	147,644	1,231	155,154	2,409	302,798
GRAND TOTAL	22,459	3,128,192	23,380	3,266,178	45,839	6,394,370

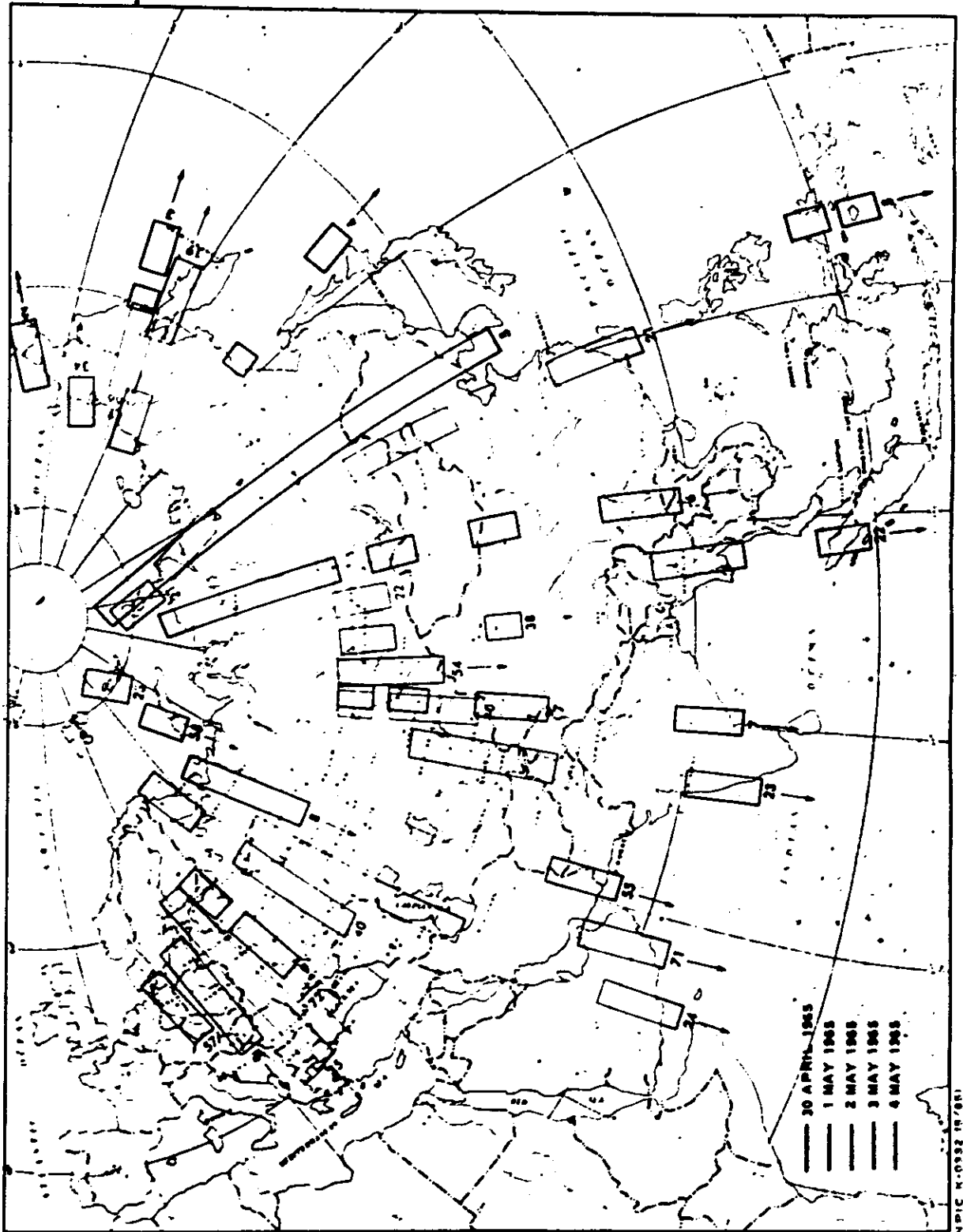
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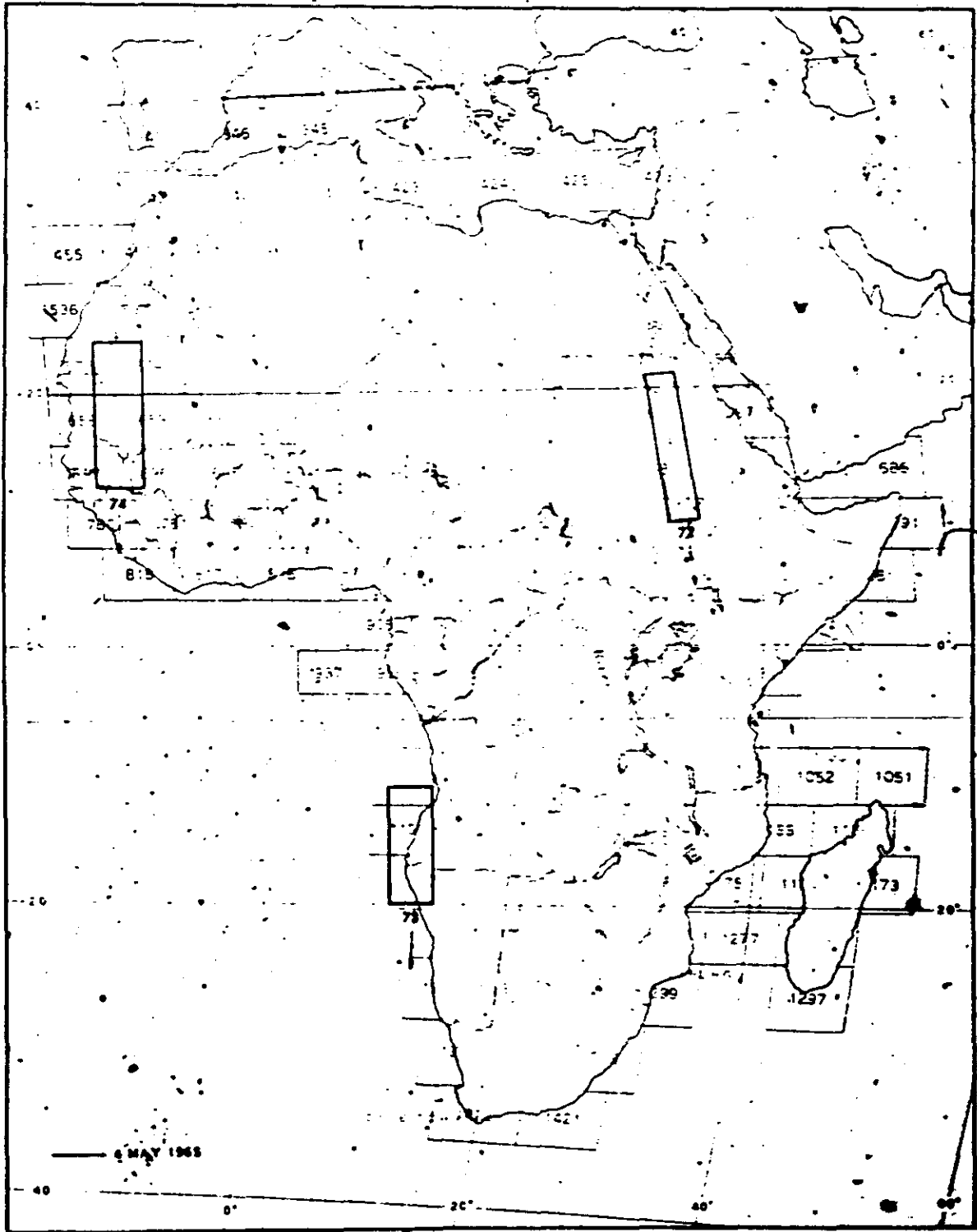


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APPROXIMATE TRACK OF MISSION 1019-1, 30 APRIL - 4 MAY 1965, OVER AFRICA.

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